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GEOTECHNICAL REPORT AMBLER AIRPORT REHABILITATION AKSAS NUMBER: 61303 and AMBLER SEWAGE LAGOON ROAD AKSAS NUMBER: 61056 JUNE 2013

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Contents

Summary
Introduction
Physical Setting7
Location
Methods 10
Laboratory Soil Testing
Subsurface Findings
 Northern Main Runway and Extension, Crosswind Runway and Terrain Obstruction Area11 Southern Main Runway and Extension, Existing Parking Apron, Taxiway and SREB23 Existing Airport Access Road and Realignment Area
Comments and Recommendations
Material Sources
Ambler Sewage Lagoon Road
Expected Physical Site Conditions
Recommendations
Material Sources
References:
APPENDIX A: TEST HOLE LOCATION MAPS, LOGS AND ORIGINAL GROUND PROFILES:
APPENDIX B: LABORTORY TEST RESULTS:
APPENDIX C: NATURALLY OCCURRING ASBESTOS LABORTORY TEST RESULTS:
APPENDIX D: THERMISTOR RESULTS
APPENDIX E: PREVIOUS TEST HOLE LOCATIONS AND RESULTS
APPENDIX F: SELECTED PHOTOS
APPENDIX G: SYMBOLS AND DEFINITIONS, UNIFIED SOIL CLASSIFICATION SYSTEM, DESCRIPTION AND CLASSIFICATION OF FROZEN SOILS

GEOTECHNICAL REPORT AMBLER AIRPORT REHABILITATION STATE PROJECT NUMBER: 61303

Summary

The Alaska Department of Transportation and Public Facilities (ADOT&PF) Northern Region design engineers are evaluating improvements to the Ambler Airport (Figure 1). Potential improvements include these design elements.

- Lengthen the existing main runway to 4,000 feet and widen to 75 feet.
- Lengthen the existing Runway Safety Area (RSA) to 4,600 feet and widen to 150 feet.
- Overlay runways, taxiway, apron, and embankments with surface course material or pavement.
- Remove terrain obstructions at the southwest corner of the intersecting runways, and use material as potential borrow.
- Construct new Snow Removal Equipment Building (SREB) at current SREB location.
- Realign 850 feet of airport access road.
- Rehabilitate and resurface 2,750 feet of airport access road.
- Construct permanent drainage structure at Grizzly Creek.

The design element to overlay the runways, taxiway and apron, embankments, including the airport access road, is dependent on the presents of Naturally Occurring Asbestos (NOA) in those areas and local material sites. Geotechnical considerations and NOA testing will determine the final overlay decision, options being considered are:

- Rehabilitate and apply crushed aggregate surface to all operational surfaces and access road using a local material source.
- Rehabilitate and apply crushed aggregate surface to all operational surfaces and access road using non-NOA material sources not in the local area.
- Rehabilitate and apply asphalt surfacing to all operational surfaces and access road.

To assist with evaluation and planning, Northern Region Materials Section (NRMS) personnel conducted a geotechnical investigation with drilling explorations for all airport improvements (Figure 2). This report presents the results of the investigation, including improvements to the Ambler sewage lagoon road. This investigation and report does not give information related to material sources, except in the terrain obstruction area. The material source investigation was completed under a separate report dated 2013.

This report will discuss each of the above mentioned design elements in separate sections, as indicated below:

- 1. Northern main runway, northern main runway extension, crosswind runway, and terrain obstruction area.
- 2. Southern main runway, southern main runway extension, existing aircraft parking apron, taxiway, and SREB.
- 3. Existing airport access road and proposed new access road realignment.
- 4. Proposed new aircraft parking apron expansion and SREB, north of the existing parking apron. This design element is no longer being considered. The existing apron is the only consideration.

5. Ambler sewage lagoon road improvements. This is discussed last under a separate project, but included in this report.



Figure 1: Ambler Airport Location and Vicinity Map.



Figure 2: Ambler Airport Improvements Design Elements.

Introduction

This report documents physical site conditions and subsurface geotechnical conditions, provides interpretation of anticipated site conditions, and recommends design and construction criteria for the project. This report is intended to serve as a geotechnical guide during project design and a geotechnical reference during construction.

The purpose of this project and the geotechnical investigation presented here is to improve safety and efficiency at the Ambler Airport. The Village of Ambler is often supplied by air freight making the airport essential to the community. The current runway length does not support fully loaded larger aircraft. In addition, the existing runway's deteriorating surface causes operational problems that result in frequent closures during the spring breakup due to soft conditions.

The existing Ambler airport (AFM) main runway with access road was originally constructed in 1978, with improvements in 1989 to include expanding the main runway to its current length and adding the crosswind runway. The main runway is currently approximately 3,000 feet in length with a 60 foot wide gravel runway surface and approximately 270 foot overruns, located 1 mile northwest of the village of Ambler at N67°06.38' and W157°51.45' and at 334 feet above mean sea level. The main runway, 18-36 is oriented northeast and southwest, with a slight slope up to the northeast and crowned in the center with no line of sight between runway ends. The crosswind runway, 09-27 is 2,400 feet in length with a 60 feet wide gravel runway surface that is often closed due to a deteriorating surface. The runway slopes uphill from east to west, and is oriented southeast and northwest (FAA Supplement Alaska, 2012).

The airport improvements and sewer lagoon road geotechnical field investigation was conducted from February 11th thru March 5th, 2013. A total of 59 test holes (TH) were drilled as part of this investigation:

- Nineteen test holes drilled on the main runway including overruns and proposed extension areas.
- Eight test holes drilled on the crosswind runway.
- Seven test holes drilled in the terrain obstruction area.
- Three test holes drilled on the existing taxiway and parking apron, including SREB area.
- Six test holes drilled on the existing airport access road, and four holes drilled in the proposed access road realignment area.
- Two test holes drilled in proposed new apron expansion area, and 5 test holes drilled in proposed new SREB area. Area is no longer considered under this project.
- Five test holes drilled on the Ambler sewer lagoon road.

To support the investigation, a total of 283 soil samples were collected from the test hole locations. Samples were collected for NOA testing, organic and moisture content testing, moisture density relationship, gradation with classification, and frozen unit weight.

Physical Setting

Location

Ambler is an Inupiat village of approximately 276 people located on the north bank of the Kobuk River, and near the confluence of the Ambler and Kobuk Rivers. Ambler is about 138 miles east of Kotzebue in northwestern Alaska, and within the boundaries of the Northwest Arctic Borough. Ambler is not linked by any road and travelling to the area is by small aircraft throughout the year with scheduled flight service from Kotzebue. The Kobuk River is navigable from early July to mid-October.

Climate

The Environmental Atlas of Alaska (Hartman, 1984) indicates the village of Ambler is located in the continental climate zone of Alaska, characterized by pronounced temperature variations throughout the day and year, low precipitation, low cloudiness, and low humidity. Surface winds are generally light with average annual wind speeds of 6.5 mph with the prevailing wind direction at NNE. The project area receives continuous sunlight or twilight from late May to late July, and almost no sunlight in December. Table 1 below is a summary of climate data for Ambler.

Average	Jan	Feb	Mar	Apr	May	Jun	Jul	Aug	Sep	Oct	Nov	Dec	Annual
Max. Temp. (F)	0.1	1.0	13.8	27.7	50.4	69.2	70.6	61.7	48.2	26.9	7.8	5.7	32.0
Min. Temp. (F)	-16.8	-19.3	-10.1	5.3	28.6	43.2	47.2	41.9	32.1	12.7	-5.9	-10.6	12.4
Total Precip. (in.)	1.22	1.13	1.04	1.34	1.41	1.41	2.91	4.52	4.18	1.73	0.82	1.71	23.42
Total Snowfall (in.)	19.7	16.7	17.6	17.2	4.1	0.0	0.0	0.0	3.7	17.9	9.6	27.5	134.0
Snow Depth (in.)	32	35	37	30	7	0	0	0	0	5	10	20	15

Table 1:	Climate Data Summary.	Ambler West (500260), period of Record:	1981 to 2010.
Snowfall	and depth data are from	December 1981 to March 1992.	

Data source: Western Regional Climate Center, wrcc@dri.edu.

The following Table 2 is the thawing and freezing index for Ambler. The thawing index, or degreedays above freezing, is a measure of thawing that occurs during the year. The thawing index listed below takes the annual thawing-degree days (TDD) for the last thirty years and averages them. The design thawing index takes the average of the three warmest (highest) TDD over the last thirty years.

Likewise, the freezing index, or degree-days below freezing, can be used to calculate the depth of ground freezing during winter. The freezing index listed below averages the annual freezing-degree-days (FDD) for the past thirty years. The design freezing index averages the three coldest (highest) FDD for the same period.

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Thawing Index	2200 Fahrenheit degree-days				
Freezing Index	6300 Fahrenheit degree-days				
Design Thawing Index	2600 Fahrenheit degree-days				
Design Freezing Index	7100 Fahrenheit degree-days				

Table 2: Thawing and Freezing Index, Ambler Alaska.

Geology and Topography

The village of Ambler is located in the Western Alaska physiographic province and within the Kobuk - Selawik and Ambler-Chandalar Ridge Lowlands (Wahrhaftig, 1965), in the northern portion of the Selawik topographic quadrangle and just south of the Baird Mountains quadrangle, both within the Kateel River Meridian. The Kobuk river lowlands consist mainly of sand and gravel broad river flood plains with numerous lakes and swampy terrain. The river is bordered by gravel and sand terraces 100 to 200 feet above the river level (Wahrhaftig, 1965).

The airport is situated on a broad alluvial fan extending from Jade Mountain at about 1.5 miles north. Jade Mountain is a small mountain range parallel to the southern slope of the Brooks Range. Bedrock within the Brooks Range and Jade Mountain are underlain primarily by metasedimentary rocks, with serpentine rocks containing asbestos mapped at the Jade Mountains. The asbestos eroded from these rocks and was transported throughout the area (Patton, 1968).

The surface geology mapped near the airport consists of well-rounded fine to coarse sand in stabilized dunes, and till and outwash gravel and sand deposits (Fernald, 1964). Moderately thick to thin continuous permafrost underlies most areas near Ambler. Discontinuous permafrost underlies areas of coarse grained deposits near the Kobuk River.

Ambler lies in an area of low seismic activity (Figure 3), and as a result falls under Seismic Zone 2B according to The Uniform Building Code, 1997 version. The United States Geological Survey Seismic hazard map from 2007 gives the area a peak ground acceleration of .10g to .25g, with a 10 percent probability of exceedance in 50 years. The mapped fault shown in red on Figure 3 is the Kobuk Fault and is mapped approximately 30 miles east of Ambler.



Figure 3: Northwestern Alaska Seismicity, Data from 1958 to 2003. Ambler is located in the lower center of the figure and west of Kobuk. Source: Alaska Earthquake Information Center. www.aeic.alaska.edu

Field Investigation

Methods

This geotechnical investigation was conducted by NRMS personnel consisting of drillers S. Parker and P. Lanigan, and engineering geologist T. Weiss. A Mobile B-24 drill mounted on a Raid Trac carrier was used to drill the test holes. The drill rig was equipped with 4.5- inch O.D. solid flight augers, and 4.4-inch O.D. hollow stem augers.

The solid flight auger drilling method was accomplished with relative ease at 43 test hole locations, with disturbed soil samples collected from the auger cuttings returned to the surface and placed into either small sized metal tins or larger sized canvas bags. As drilling proceeded, temperatures of the drill cuttings were selectively tested with a Fisher Scientific digital hand held thermometer and recorded on the test hole logs.

More detailed drilling and soil sampling was accomplished at 16 selected locations using the hollow stem auger method and two different soil samplers depending on drilling conditions. The samplers are a 1.25-inch I.D. five feet in length split-barrel continuous drill core sampler with a cutting bit used in frozen material, and a 1.25- inch I.D. two feet in length split-spoon sampler used in thawed material, when encountered. Both samplers were lowered inside the hollow stem auger.

Continuous drill core samples were relatively undisturbed, except when tightly frozen silt material was encountered. Frictional heat from drilling often thawed the outside of the samples and in some cases completely. Disturbed samples were collected with the split-spoon sampler when thawed material was encountered. The sampler was driven using a 140 pound safety hammer and 30-inch free-fall distance using a hydraulic cathead and rope. The penetration resistance was recorded by hammer blow counts as the sampler advanced every 6-inchs to two feet in depth.

Recovered samples were photographed and the temperature was recorded. Samples were placed into canvas bags, plastic bags, or metal tins sealed with vinyl tape. Most frozen core samples were stored in a frozen state through transport until laboratory testing.

Two test holes were selected to receive thermistor strings, these test holes were TH13-019 drilled on the main runway and TH13-065. TH13-065 was drilled in the area to the northeast of the existing parking apron and once considered for a new SREB, but no longer a part of this project. The thermistor strings were Digital Temperature Acquisition Cables (TAC) and manufactured by BeadedStream Services LLC in Anchorage, Alaska. After completion of drilling and logging of the test hole subsurface soil conditions, a $\frac{1}{2}$ -inch PVC pipe was placed in the hole and backfilled with auger cuttings. The TAC was lowered down the pipe and a solar powered data logger was connected to the TAC. The TAC at TH13-019 had a total length of 27 feet, with a 10 foot lead and temperature sensors spaced at 1, 2, 2, 2, 5 and 5 feet apart. The TAC at TH13-065 had a total length of 42 feet, with a 10 foot lead and temperature sensors spaced at 1, 2, 2, 2, 5, 5, 5, 5, and 5 feet apart. The results of these thermistor strings and recordings from them are given in Appendix D.

Drilling and test hole conditions were logged in the field using the Unified Soil Classification System (USCS). Test hole logs are presented in Appendix A, with a key to the logs and the USCS in Appendix G. All test hole locations were recorded using a hand held Global Positioning System (GPS), Garmin GPS 72 model using the North American Datum (NAD) 83. The GPS has an

accuracy of plus or minus 50 feet. After drilling and sample collection, all test holes were backfilled with auger cuttings to the surface and tamped flush.

Laboratory Soil Testing

Laboratory analysis of selected representative soil samples was conducted by the Northern Region Materials Laboratory (NRML), and Shannon and Wilson, Inc in Fairbanks. The testing program by NRML included gradations with classification, moisture and organic content analysis, moisture density relationship (Proctor), and liquid and plastic limits. The laboratory testing program by NRML was performed in accordance with the test methods indicated below in Table 3. Laboratory testing of frozen soil core samples were accomplished by Shannon and Wilson, and testing included dry and wet frozen unit weights and moisture content analysis.

Test Method	AASHTO	ASTM
In	dex Tests	•
Gradation	T27	C136
Minus #200 Gradation	T11	C117
Hydrometer	T88	D422
Liquid Limit	Т89	D4318
Plastic Limit	Т90	D4318
Moisture Content – Aggregate	T255	C566
Soil	T265	D2216
Organic Content (Burn)	T267	
Proctor	T180	D1557
USCS Classification	D24	87
Fine Specific Gravity	T100	D854
Coarse Specific Gravity	Т85	D127

 Table 3: Northern Region Material Laboratory Test Methods.

Small metal tin samples were collected for NOA testing at most test hole locations within approximately seven feet of the surface at the runways, access road, lagoon road, and parking apron and taxiway locations. Samples were sealed in the field shortly after collection and transported upon completion of field work. The samples were then packaged into groupings of approximately 20 and shipped to EMSL Analytical, Inc. in San Leandro , CA for asbestos testing in accordance with the California Air Resources Board (CARB) 435 Transmission Electron Microscopy (TEM) method level B with a sensitivity of 0.1 percent. The samples at the lab are crushed using a mill to produce a material of which the majority is less than 200 Tyler mesh (0.75 microns). The analytical results are reported in percent asbestos as derived from a 400 point counting technique (EMSL, 2013). The results of this NOA testing are summarized in Appendix C, which includes a chart indicating depth of sample, NOA results in number of asbestos structures found, and sample location by design element.

Subsurface Findings

1. Northern Main Runway and Extension, Crosswind Runway and Terrain Obstruction Area

The northern end of the main runway is proposed to be lengthened 800 feet and widened to 75 feet with the RSA widened to 150 feet. Both the crosswind and main runways are proposed to be

resurfaced with surface course material or pavement (Figure 4). A terrain obstruction area between the main and crosswind runways and at the southwest corner of the intersection of the two, does not allow for clear line of site visibility. The area is proposed to be cleared and reduced in elevation to allow for better visibility (Figure 5).



Figure 4: Main and Crosswind Runway Rehabilitation Typical Section.

Test holes drilled for the northern portion of the main runway, extension area, and crosswind runway were spaced from approximately 250 to 400 feet apart, (Figure 5) and (Appendix A). One test hole, TH13-011 originally planned for the obstruction area was moved to the toe of the crosswind runway embankment, but still shown as part of the obstruction area drilling. All test holes were drilled from 14.5 to 30 feet in depth. Test holes drilled for each of the design elements and the subsurface finding are discussed in the order given below:

- Seven test holes (TH13-004 to 006, 008, 044, 046 and 019) were drilled along the northern portion of the main runway including the intersection of the main runway with the crosswind runway.
- Three test holes (TH13-001 to 003) drilled for the northern main runway extension area.
- Eight test holes (TH13-012 to 016, 045, 007 and 047) drilled along the crosswind runway.
- Seven test holes (TH13-009 to 011, 017, 018, 048 and 049) drilled in the terrain obstruction area.

Test hole subsurface finding will be summarized below, with a summary of previous geotechnical investigations included. All test hole logs are presented in Appendix A, with complete laboratory test

results in Appendix B. Asbestos sample test results are shown in Appendix C, and thermistor results in Appendix D. All previous geotechnical investigations logs, laboratory results and profiles are given in Appendix E. Additional photographs are presented in Appendix F.



Figure 5: Northern Main Runway and Extension, Crosswind Runway, and Terrain Obstruction Area with Test Hole Locations.

A. Northern Main Runway Subsurface Findings

The northern portion of the main runway is gradually sloping from south to north, and at the time of our investigation snow was pushed from east to west and piled along the western edge. Snow piles were largest at the intersection with the crosswind runway.

The embankment on the western side of the runway is at or slightly below the elevation of original ground. The embankment on the east side is 8 to 15 feet above original ground, and the terrain at the toe of the embankment is uneven with some low depressions (Figure 6). The main runway was originally built between cut and fills from south to north and from west to east, as indicated from asbuild drawings from 1978 and 1989 and presented in Appendix E. A profile of original ground elevation is presented in Appendix A with existing ground elevation, test hole locations and logs.



Figure 6: Northern portion of the main runway and the eastern embankment slope looking north. The main runway is shown on the left, with the eastern portion of the crosswind runway in the background. Photo is taken near TH13-019 with a low depression area shown at the toe of the embankment in the center of the picture.

Test holes located on the runway or safety overrun areas of the northern main runway were drilled up to 50 feet left or right of centerline. TH13-005, 046, and 019 were drilled with the hollow stem auger method, and the remaining drilled solid stem auger method. These seven test holes encountered the following subsurface conditions:

- Approximately 6 inches thick base course (surface layer) material consisting of frozen silty sand with gravel.
- Thawed material was encountered from 9.5 to 16 feet in depth at TH13-004, 11.0 to 12.5 at TH13-019, and TH13-008 from 7 to 9 feet in depth.
- Moisture content samples in thawed material and only from TH13-004 indicated 11.5 and 17. 5 percent, with organic content at 0.6 percent.
- Seasonal frost material was encountered from the surface to depths of 7 to 11 feet. Permafrost was encountered from 9 to 16 feet in depth. TH13-046, 044, 006, and 005 were frozen to depths explored, and therefore permafrost depth could not be determined.
- Moisture contents in the frozen material ranged from 4.9 to 25.3 percent.
- Organic contents in frozen material were slight and ranged from 0.3 to 3 percent.
- Asbestos sample results ranged from 0.2 percent by weight (74 asbestos structures) to less than 0.1 percent by weight (zero structures). The highest asbestos results are given below with test hole number and depth, and the number of asbestos structures found larger than one per sample and percent by weight:
 - 1. TH13-006 at 0.5 feet in depth and 74 structures or 0.2 percent by weight.
 - 2. TH13-019 at 1 foot in depth and 36 structures or less than 0.1 percent by weight.

- 3. TH13-005 at 4.3 feet and 8 structures or less than 0.1 percent by weight.
- 4. TH13-004 at 2.5 feet and 3 structures or less than 0.1 percent by weight.
- 5. TH13-006 at 2.5 feet and 3 structures or less than 0.1 percent by weight.
- 6. TH13-008 at 5 feet and 3 structures or less than 0.1 percent by weight.

Visible Ice was not encountered in any test holes on the northern main runway to the depths explored. Frozen material encountered was classified as nonvisible bonded with no excess ice (Nbn), nonvisible bonded with excess ice (Nbe), and poorly bonded or friable (Nf). See Appendix G for a key to frozen ground classification. Groundwater or perched water was not encountered in any test holes.

Soil material described in the field or classified as silty sand or sandy silt was mostly fine sand. The material met little resistance during drilling. This is in contrast to well bonded frozen silt, silt with sand, or sandy silt material that was mostly difficult to drill, and at some locations caused auger refusal. Auger refusal was generally encountered near the intersection of the main runway with the crosswind runway. Photos of the two different materials are included in Appendix F.

Selected laboratory test results for the northern portion of the main runway are summarized below in Table 4. The table also indicates frozen material depth, and depth to original ground indicating cut or fill depth from the original main runway profile shown in Appendix A and E.

Test Hole and Station	Hole Depth (feet)	Percent Passing #200	Frozen Material Depth (feet)	Moisture Content (%)	Cut/Fill (feet)
TH13-019\36+00	20		0-11\12.5-20	13.0,6.5,9.4	Fill 8
TH13-008\40+00	16		0-7\9-16	25.1,24.6,28.0	Fill 2
TH13-046\42+00	15		0-15	4.9, 19.4	Cut 1.5
TH13-006\43+50	15	85.6	0-15	22.6,25.3	Fill 2
TH13-044\46+50	20		0-20	16.8,9.4,11.6	Cut 4
TH13-005\48+00	14.5	76.4,75.5,72.7	0-14.5	20.4,21.0,22.0	Fill 11
TH13-004\50+50	20	46.6	0-9.5\16-20	12.8,11.4,17.5,20.9	Fill 21

 Table 4: Summary of Selected Laboratory Test Results from Test Holes at the Northern

 Portion of the Main Runway.

Table 5 below is the laboratory test results for frozen unit weight testing provided by Shannon and Wilson, Inc. in Fairbanks. The table also indicates the material classification for each sample.

Test Hole\ Station	Sample Depth (feet)	Moist Unit Weight (pcf)	Dry Unit Weight (pcf)	Gravimetric Moisture Content (%)	Material Classification
TH13-046/42+00	5 - 10	119.6	93.0	28.7	Silt w/sand
TH13-019/36+00	15 - 20	101.7	90.7	12.1	silty Sand

 Table 5: Northern Main Runway Frozen Unit Weight of Soil Test Results.

A scatter plot of the relationship between sample moisture content and depth is represented below in Figure 7 for all test hole locations and samples collected along the main runway including the southern portion. The thick black line is the best-fit linear trend line of the values with the calculated equation displayed near the line.



Figure 7: Main Runway Moisture Content verses Depth Chart with Trend Line.

B. Proposed Northern Main Runway Extension Subsurface Findings

Test holes located for the proposed northern main runway extension area were drilled on a gradual to moderate slope extending out from the end of the exiting runway embankment to the north. TH13-003 was drilled near the crest of the slope and TH13-002 near the toe. TH13-001 was drilled on a slope that appeared to be natural (Figure 5 and Appendix A). At the time of our field work snow was approximately two to three feet deep, but a trail was cleared to provide better drill rig access. TH13-001 was drilled using the hollow stem auger method. The three test holes encountered the following subsurface conditions:

- One foot thick organic mat at TH13-001 and 002.
- Thawed material from 5.5 to 9 feet in depth at TH13-001, and from 12 and 13 feet to the depth explored at 20 feet in TH13-002 and 003.
- Moisture contents in thawed material ranged from 9.3 to 29.7 percent, with the highest moisture content sampled from TH13-001 and appeared to be associated with a perched water table. Two organic contents indicated 0.9 and 1.7 percent.
- Seasonal frost material was encountered from the surface to 5.5 feet in depth at TH13-001, and 12 and 13 feet at TH13-002 and 003 respectively. Permafrost was encountered in TH13-001 from 9 feet to the depth explored at 20 feet.

- Moisture contents in the frozen material ranged from 6.8 to 38.3 percent. The higher moisture content results were also encountered in TH13-001.
- Organic contents in frozen material were slight and ranged from 0.6 to 1.0 percent.
- Two asbestos samples collected at TH13-003 from 1 foot and 4.5 feet in depth, indicated less than 0.1 percent by weight and 14 asbestos structures, and less than 0.1 percent by weight and 1 asbestos structure, respectively.

Visible Ice was not encountered in any northern main runway extension test holes to the depths explored. Frozen material encountered was classified as nonvisible bonded with no excess ice (Nbn), nonvisible bonded with excess ice (Nbe), and poorly bonded or friable (Nf). See Appendix G for a key to frozen ground classification.

Selected laboratory test results for the northern main runway extension area are summarized below in Table 6. The table also indicates frozen material depth, and depth to original ground indicating cut or fill depth from the original main runway profile.

Table 6: Summary of Selected Laboratory Test Results for Test Holes at the Proposed Northern Main Runway Extension Area.

Test Hole and Station	Hole Depth (feet)	Percent Passing #200	Frozen Material Depth (feet)	Moisture Content (%)	Cut/Fill (feet)
TH13-003\52+50	20	69.1	0-13	8.3,8.4,14.1	Fill 20
TH13-002\55+50	20		0-12	11.5,6.8,9.3,11.5	None
TH13-001\58+00	20		0-5.5\9-20	29.7,38.3,31.4	None

Table 7 below is the laboratory test results for frozen unit weight testing from samples at TH13-001, and provided by Shannon and Wilson, Inc. in Fairbanks. The table also indicates the material classification for each sample.

 Table 7: Proposed Northern Main Runway Extension Area, Frozen Unit Weight of Soil Test

 Results.

Test Hole\ Station	Sample Depth (feet)	Moist Unit Weight (pcf)	Dry Unit Weight (pcf)	Gravimetric Moisture Content (%)	Material Classification
TH13-001\58+00	0 - 5	75.1	*27.8	170.1	Silt w/sand
TH13-001	0 - 5	113.4	76.9	47.5	Silt w/sand
TH13-001	10 - 14.5	119.6	87.3	37.0	sandy Silt
TH13-001	15 - 19	117.8	86.5	36.2	sandy Silt

* numerous organics associated with surficial topsoil.

C. Crosswind Runway Subsurface Findings

The crosswind runway was snow covered and closed at the start of our investigation. Due to the possible conflict of our drilling work with landing aircraft, the crosswind runway was plowed and opened. The surface of the crosswind runway appeared to be in good condition. However, the

runway maintenance person in Ambler, Mr. Alvin Williams, stated the crosswind runway is mostly closed during the summer due to pot holes, cracking and voids. Mr. Williams also stated that most damage to the runway occurs between TH13-012 to TH13-014, and just west of the intersection with the main runway and near TH13-007.

According to as-built drawings the crosswind runway was built approximately 10 years after the original main runway construction, and was built with a deep fill between cut areas as indicated in Appendix A and E.

TH13-045 was drilled on the crosswind runway and east of the main runway, all the other seven test holes were drilled to the west of the main runway (Figure 5 and Appendix A). Test holes located on the runway or overrun areas of the crosswind runway were drilled left or right of centerline with some near the edge of the embankment. TH13-047, 013 and 016 were drilled using the hollow stem auger method, and the remaining test holes using the solid stem auger method. These eight test holes encountered the following subsurface soil conditions:

- Approximately 6 inches thick base coarse material consisting of frozen silty sand with gravel.
- Thawed material was encountered from 16.5 to 27.5 feet in TH13-045, and 13.0 feet to the depth explored at 20 feet in TH13-012.
- Moisture contents in thawed material indicated 6.5 and 17.3 percent in TH13-012 and TH13-045, respectively, with one organic content at 0.2 percent in TH13-045.
- Seasonal frost material was encountered from the surface to 13 and 16.5 feet in depth in TH13-012 and 045, respectively. Permafrost was encountered in TH13-045 at 27.5 feet to the depth explored at 30 feet and consisted of silt with sand material. TH13-007, 047, 013, 014, 015 and 016 were all frozen to depths explored, and therefore permafrost depth could not be determined.
- Moisture contents in the frozen material ranged from 14.2 to 32.5 percent, with higher moisture contents encountered in TH13-014 and 013. These test holes were located in the fill area of the crosswind runway.
- Organic contents in frozen material were slight and ranged from 0.2 to 1.0 percent.
- Asbestos sample results ranged from 0.1 percent by weight and 23 asbestos structures to less than 0.1 percent by weight and 0 asbestos structures. The highest asbestos results are given below with test hole number and depth, and the number of asbestos structures found larger than one per sample:
 - 1. TH13-016 at 1.5 feet in depth and 23 structures and 0.1 percent by weight.
 - 2. TH13-007 at 1 foot in depth and 5 structures and less than 0.1 percent by weight.
 - 3. TH13-015 at 5.5 feet and 3 structures and less than 0.1 percent by weight.

Visible Ice was not encountered in any crosswind test holes to the depths explored, Frozen material encountered was classified as nonvisible bonded with no excess ice (Nbn), nonvisible bonded with excess ice (Nbe), and poorly bonded or friable (Nf). Groundwater was not encountered in any test hole locations.

TH13-011 was drilled at the toe on the south side of the crosswind runway embankment, and in a low area adjacent to the terrain obstruction area (Figure 5 and Appendix A). This test hole was moved slightly to provide subsurface information at the toe of the crosswind runway embankment. The test hole encountered:

- 1 foot thick organic mat.
- Silty sand material from 1 foot to the depth explored at 20 feet.

- Seasonally frozen material to 12.5 feet and thawed to 20 feet.
- Moisture contents indicated 16.7 percent at 10 feet, 25.5 percent at 13.5 feet, and 29.1 percent at 19 feet in depth.

Selected laboratory test results for the crosswind runway are summarized below in Table 8. The table also indicates frozen material depth, and depth to original ground indicating cut or fill depth from the original crosswind runway profile.

Test Hole and Station	Hole Depth	Percent Passing #200	Frozen Material	Moisture Content (%)	Cut/Fill (feet)
	(feet)		Depth (feet)		
TH13-045\504+00	30	82.8	0-16.5\27.5-	12.2,20.2,13.4,17.3,19.3	Fill 10
			30		
TH13-007\507+00	20	91.0	0-20	15.5,22.7,25.6,	Fill 3
TH13-047\511+50	20		0-20	21.2,11.1,6.2,24.2	Cut 10
TH13-012\515+00	20		0-13	23.5,14.2,15.0,6.5	Fill 9
TH13-011\516+00	20		0-12.5	16.7,25.5,29.1	None
TH13-013\518+50	20	90.5	0-20	26.6,23.1	Fill 10
TH13-014\521+50	20	92.3,91.6,79.4	0-20	32.5,28.7	Fill 8
TH13-015\525+50	15	45.1,93.0	0-15	17.5,22.0,25.2	Cut 6
TH13-016\529+00	20	66.5	0-20	15.4,12.7,10.8	Cut 6

 Table 8: Summary of Selected Laboratory Test Results from Test Holes at the Crosswind Runway.

Table 9 below is the laboratory test results for frozen unit weight testing from samples collected at the crosswind runway, and provided by Shannon and Wilson, Inc. in Fairbanks. The table also indicates the material classification for each sample.

Test Hole\ Station	Sample Depth (feet)	Moist Unit Weight (pcf)	Dry Unit Weight (pcf)	Gravimetric Moisture Content (%)	Material Classification
TH13-047\511+50	5 - 10	127.6	101.9	25.3	silty Sand
TH13-047	15 - 19.5	118.4	91.1	29.9	silty Sand
TH13-013\518+50	10 - 15	121.4	97.9	24.0	sandy Silt
TH13-013	15 - 20	126.5	93.9	34.6	sandy Silt

Table 9: Crosswind Runway Frozen Unit Weight of Soil Test Results.

A scatter plot of the relationship between sample moisture content and depth is represented below in Figure 9 for all test hole locations and samples collected along the crosswind runway. The thick black line is the best-fit linear trend line of the values with the calculated equation displayed near the line.



Figure 9: Crosswind Runway Moisture Content verses Depth Chart with Trend Line.

D. Terrain Obstruction Area Subsurface Findings

The terrain obstruction area at the southwest corner of the main and crosswind runways is up to approximately 10 feet higher in elevation than the runways, and does not provide visibility between the two. The area has an undulating surface with spruce trees up to 6 inches in diameter and overall gradually slopes to the south and southwest. TH13-048 is located in a distrubed area and lower in elevation than areas to the north, this area could have distrubance related to a nearby weather station and antennas. The obstruction area was snow covered at the time of our investigation with up to 3 feet of snow and some drifting. A small trail was plowed to provide drill rig access.

We located test holes in the terrain obstruction area to determine the use of the excavated material as borrow. TH13-011 was located to provide subsurface information in a low area and near the toe of the crosswind runway embankment (Figure 5 and Appendix A). All test holes were drilled using the solid stem auger method. These seven test holes encountered the following subsurface conditions:

- 1 foot thick organic mat.
- Thawed material was encountered in all test holes except TH13-048, and at depths from 12 to 12.5 feet and continued to the depths explored at 15 feet. The depth to thawed material was relatively consistent, and material consisted of silt and fine silty sand. Temperatures were recorded in drilled auger cuttings and consistently changed at the 12 foot depth, indicating the transition to thawed soil.
- Moisture contents in thawed material ranged from 8.9 to 29.1 percent. Higher moistures were collected from TH13-011, located at the toe of the crosswind runway embankment and in a low area.
- Seasonally frozen material was encountered from the surface to 12 feet in depth. Permafrost was not encountered in any test holes. TH13-048 was frozen to the depth explored at 15 feet and therefore permafrost depth could not be determined.

- Moisture contents in the frozen material ranged from 7.5 to 16.7 percent. Higher moisture contents were encountered in TH13-048 with 28.4 and 31.8 percent collected in silt material, and a high organic layer from 2 to 5 feet in depth yielded a moisture content of 115.5 percent.
- Organic contents in frozen material were slight and ranged from 0.2 to 1.1 percent. At TH13-048 the high organic material encountered from 2 to 5 feet indicated 44.0 percent organics.
- Asbestos sample results ranged from less than 0.1 percent by weight and 12 asbestos structures to less than 0.1 percent by weight and zero asbestos structures. The highest asbestos results are given below with test hole number and depth, and the number of asbestos structures found larger than one per sample:
 - 1. TH13-018 at 2 feet in depth and 12 structures and less than 0.1 percent by weight.
 - 2. TH13-049 at 3 feet in depth and 2 structures and less than 0.1 percent by weight.

Visible Ice was not encountered in any test holes in the terrain obstruction area to the depths explored. Frozen material encountered was classified as nonvisible bonded with no excess ice (Nbn), nonvisible bonded with excess ice (Nbe), and poorly bonded or friable (Nf).

Selected laboratory test results for the terrain obstruction area are summarized below in Table 10. The table also indicates frozen material depth, and depth to original ground indicating cut or fill depth from the original main runway profile.

Test Hole and Station	Hole Denth	Percent Passing #200	Frozen Material	Moisture Content (%)	Cut/Fill (feet)
	(feet)		Depth (feet)		0
TH13-009\40+50	15	85.0	0-12	11.7,8.9	None
TH13-010\512+50	15	50.2,45.3	0-12	7.5	None
TH13-011\516+00	20		0-12.5	16.7,25.5,29.1	None
TH13-017\38+00	15		0-12	10.9,14.9	None
TH13-018\35+50	15	62.9	0-12		None
TH13-048\36+50	15		0-15	115.5,31.8,28.4	None
TH13-049\515+00	15	51.4	0-12.5	9.4	None

 Table 10: Summary of Selected Laboratory Test Results from Test Holes Located in the

 Terrain Obstruction Area.

E. Previous Geotechnical Investigations Subsurface Findings

Previous airport geotechnical investigations were accomplished in 1973, 1985 and 1986. The 1973 investigation was for the original main runway and included the 2,600 foot main runway with 250 foot safety overrun to the north and 150 foot safety overrun to the south, parking apron and airport access road. The 1985 and 86 investigations included the crosswind runway, main runway expansion to 3,000 feet with 250 foot safety overruns, and expanding the parking apron. The 1973 investigation was performed in July and included drilling seven test holes along the main runway to depths of 15 to 25 feet. The 1985 investigation was drilled in September. A summary of these previous test holes are given below in Table 11 with locations shown in Appendix E. The table also indicates frozen

material depth, and depth to original ground indicating cut or fill depth from the original main runway profile.

Test Hole and Station	Hole Depth	Percent Passing #200	Frozen Material	Moisture	Cut/Fill
	() e e i)	1 ussing #200	Depth (feet)	Comeni (70)	() e e i)
TH73-16\19+90	20	65.8	None		At Transition
TH73-17\24+00	15		None		At Transition
TH73-18\28+00	15		None		Cut 4
TH73-19\32+00	15		None		Fill 7.5
TH73-20\36+00	25	79.3	12		Fill 8
TH73-21\40+00	15	81.8	None	13.7	Fill 1.5
TH73-22\44+00	15		7		Fill 2
TH85-6\22+00	15		11.5		Cut 6
TH85-7\26+00	11	66.0	8.5	17.1	Fill 14.5
TH85-8\30+00	11		9.5		Cut 5.5
TH85-9\34+00	11		9.5		Fill 3.5
TH85-10\38+00	11	60.0	9	13.2	Fill 6.5
TH85-11\42+00	11		9		Cut 1
TH85-12\45+00	11	00000000000000000000000000000000000000	10		Fill 0.5

Table 11: Summary of Previous Test Hole Locations, Main Runway.

The investigations performed in 1985 and 86 included eight test holes drilled for the crosswind runway and one hole near the eastern end, and all drilled to depths of 15 to 23 feet. The 1985 test holes were drilled and logged in September and in July for the 1986 investigation. A summary of these holes are shown below in Table 12 with locations and additional information in Appendix E. The table also indicates frozen material depth, and depth to original ground indicating cut or fill depth from the original crosswind runway profile.

Test Hole and	Hole Depth	Percent	Frozen	Moisture	Cut/Fill
Station	(feet)	Passing #200	Material	Content (%)	(feet)
			Depth (feet)		
TH85-13\501+50	15	87.0	None	13.1	Fill 3
TH85-15\509+00	23	64.0	1.5	13.0,13.7,9.6	Cut 12
TH85-16\513+00	15	51.0	1.5	11.2	At Transition
TH85-17\517+00	17		None	19.7,30.2	Fill 12
TH85-18\522+00	15		14		Fill 6
TH86-1\519+50	15		None	35.0	Fill 12
TH86-2\524+50	15	95.0	4	13.8	Cut 3
TH86-3\528+00	15	87.0	4	10.6	Cut 12
TH86-4\530+00	15	70.0	4	5.1	Cut 10

Table 12: Summary of Previous Test Hole Locations, Crosswind Runway.

2. Southern Main Runway and Extension, Existing Parking Apron, Taxiway and SREB

The southern end of the main runway is proposed to be lengthened by 800 feet and widened to 75 feet with the RSA widened to 150 feet. The runway, existing apron and taxiway area are proposed to be resurfaced with surface coarse material or pavement. The existing SREB is located at the southeast corner of the parking apron (Figure 10).

Test holes drilled for the southern portion of the main runway, existing aircraft parking apron, taxiway and SREB area were spaced from approximately 200 to 300 feet apart, and drilled from 16 to 35 feet in depth. Test holes drilled for each of the design elements and discussed in order are:

- Six test holes (TH13-020 to 023, 050 and 051) drilled along the southern portion of the existing runway.
- Three test holes (TH13-024 to 026) drilled for the main runway southern extension area.
- One test hole (TH13-053) drilled on the existing taxiway.
- Two test holes (TH13-053 and 054) drilled on the existing aircraft parking apron and SREB area.

Test hole subsurface finding will be summarized below, with a summary of previous geotechnical investigations included. All test hole logs are presented in Appendix A, with complete laboratory test results in Appendix B. Asbestos sample test results are shown in Appendix C, and thermistor results in Appendix D. All previous geotechnical investigations logs, laboratory results and profiles are given in Appendix E. Additional photographs are presented in Appendix F.

A. Southern Main Runway Subsurface Findings

The southern portion of the main runway gradually slopes up from south to north, and at the time of our investigation snow was pushed from east to west and piled along the western edge. The embankment on the western side of the runway is at or slightly below the elevation of original ground, with a low area to the west near TH13-022. Original ground at the toe of the embankment on the east side is uneven with possible fill material spread over an area to the north of the existing parking apron and taxiway, and near TH13-021. The embankment is 10 to 20 feet higher than original ground at the southern end of the existing runway. The main runway was originally built between cut and fills from south to north and from west to east, as shown in Appendix E with as-build drawings from 1978 and 1987.

Test holes located on the runway or safety overrun areas of the southern main runway were drilled from up to 30 feet left or right of centerline. TH13-050 and 022 were drilled using the hollow stem auger method. The six test holes encountered the following subsurface conditions:

- Approximately 6 inches to two feet thick base course (surface layer) material consisting of frozen silty sand with gravel.
- Thawed material was not encountered in any test holes.
- Frozen material was encountered throughout all six test holes to depths drilled at 20 feet, and therefore the boundary between seasonal frost and permafrost depth could not be determined.
- Soil temperatures recorded from drilled auger cuttings ranged from 30.7 to 31.9 degrees Fahrenheit.



Figure 10: Southern Main Runway and Extension, Existing Aircraft Parking Apron, Taxiway and SREB with Test Hole Locations.

- Soil temperatures recorded in core samples ranged from 30.4 to 31.6 degrees Fahrenheit.
- Moisture contents in the frozen material ranged from 6 to 41 percent.
- Organic contents in frozen material were slight and ranged from 0.5 to 2 percent.
- Asbestos sample results ranged from less than 0.1 percent by weight and 50 asbestos structures to less than 0.1 percent by weight and zero structures. The highest asbestos results are given below with test hole number and depth, and the number of asbestos structures found larger than one per sample:
 - 1. TH13-021 at 1.5 feet in depth and 50 structures and less than 0.1 percent by weight.
 - 2. TH13-020 at 7 feet in depth and 43 structures and less than 0.1 percent by weight.
 - 3. TH13-021 at 6.5 feet and 22 structures and less than 0.1 percent by weight.

Visible Ice was not encountered in any test holes located on the southern main runway to the depths explored. Frozen material was classified as nonvisible bonded with no excess ice (Nbn) and poorly bonded or friable (Nf). Groundwater or a perched water table was not encountered.

Selected laboratory test results for the southern portion of the main runway are summarized below in Table 13. The table also indicates frozen material depth, and depth to original ground indicating cut or fill depth from the original main runway profile. A scatter plot of moisture content versus depth is represented in Figure 7 for all test hole locations along the main runway.

I OI HOIL ON CHO IVIN	III ACCUITY				
Test Hole and Station	Hole Depth (feet)	Percent Passing #200	Frozen Material Depth (feet)	Moisture Content (%)	Cut/Fill (feet)
TH13-023\19+50	20	67.5	0-20	25.0,12.5	Fill 1
TH13-022\25+00	20		0-20	6.0,41.1,19.7,26.9,14.2	Fill 4
TH13-021\28+00	20	57.0	0-20	6.0,6.4	Cut 4
TH13-020\33+50	20	78.9	0-20	19.2,27.8,27.5	Fill 4
TH13-051\23+00	20		0-20	17.8,20.0,22.9	Cut 4
TH13-050\30+50	20		0-20	7.1,18.6,18.2,28.2	Cut 2.5

 Table 13: Summary of Selected Laboratory Test Results from Test Holes at the Southern

 Portion of the Main Runway.

Table 14 below is the laboratory test results for frozen unit weight testing from samples collected at the southern portion of the main runway, and provided by Shannon and Wilson, Inc. in Fairbanks. The table also indicates the material classification for each sample.

Test Hole\ Station	Sample Depth (feet)	Moist Unit Weight (pcf)	Dry Unit Weight (pcf)	Gravimetric Moisture Content (%)	Material Classification
TH13-050\30+50	10 - 14.5	120.9	92.5	30.7	Silt w/sand
TH13-050	15 - 19	123.7	95.3	29.8	sandy Silt
TH13-022\25+00	10 - 15	130.7	105.8	23.5	sandy Silt
TH13-022	15 - 19.5	119.0	93.7	27.0	sandy Silt

Table 14: Southern Main Runway Frozen Unit Weight of Soil Laboratory Test Results.

B. Proposed Southern Main Runway Extension Subsurface Findings

The proposed southern main runway extension area is 10 to 20 feet lower in elevation than the existing runway, with a moderate sloping embankment. TH13-024 was located near the crest of the embankment and TH13-025 near the toe (Figure 10). At the time of our investigation snow was 2 to 4 feet in depth and a road was plowed to each location. The area around TH13-025 and TH13-026 has moderately thick vegetation consisting mostly of brush, with the airport access road between the two test holes.

Test holes located in the southern main runway extension area were drilled up to approximately 25 feet left or right of the proposed centerline. TH13-025 was drilled using the hollow stem auger method. The three test holes encountered the following subsurface conditions:

• Six inches to 1 foot organic mat.

- Thawed material was encountered in TH13-026 from 13 to the depth explored at 35 feet, and 18.5 to the depth explored at 20 feet in TH13-024.
- Moisture contents in thawed material indicated 7 and 8 percent. Visible higher moisture was encountered in TH13-026 from approximately 22 feet to the depth explored at 35 feet.
- Seasonally frozen material was encountered from the surface to 13 and 18.5 feet at TH13-026 and TH13-024, respectively. TH13-025 encountered frozen material throughout to the depth explored at 20 feet. Permafrost depth could not be determined from any of the three test holes. Frozen material consisted of sandy silt and fine silty sand.
- At TH13-026 and 024 soil temperatures recorded from drilled auger cuttings ranged from 28.7 to 41.2 degrees Fahrenheit.
- At TH13-025 temperatures recorded in soil core samples ranged from 31.4 to 32.2 degrees Fahrenheit.
- Moisture contents in frozen material ranged from 5.4 to 27.9 percent. The higher moisture content was sampled from the bottom of TH13-025 at 19.5 feet.
- Organic contents were slight and ranged from 0.5 to 0.6 percent.
- Asbestos results from one sample collected at TH13-026 and four feet in depth indicated less than 0.1 percent by weight and zero asbestos structures.

Visible Ice was not encountered in any test holes on the southern main runway extension area to the depths explored. Frozen material was classified as nonvisible bonded with no excess ice (Nbn) and poorly bonded or friable (Nf). Groundwater or a perched water table was not encountered, but may exist at depth in TH13-026.

SPT blow counts from the hollow stem auger test hole drilled at TH13-025 and from 10 to 12 feet in depth indicated 3, 5, 4 and 5 blow counts per each six inches the sampler was driven. The sample and blow counts given were performed in marginally frozen silty sand material.

Selected laboratory test results for the southern main runway extension area are summarized below in Table 15. The table also indicates frozen material depth, and depth to original ground indicating cut or fill depth from the original main runway profile.

Test Hole and Station	Depth (feet)	Percent Passing #200	Frozen Material Depth (feet)	Moisture Content (%)	Cut/Fill (feet)
TH13-026\12+50	35	69.0	0-13	5.4, 7.0	None
TH13-025\15+00	20		0-20	10.2,10.4,7.5,27.9	None
TH13-024\18+00	20		0-18.5	9.5,8.1,5.4,8.0	Fill 2

Table 15: Summary of Selected Laboratory Test l	Results from Test Holes	at the Southern Main
Runway Extension Area.		

Table 16 below is the laboratory test results for frozen unit weight testing from samples collected at the southern main runway extension area, and provided by Shannon and Wilson, Inc. in Fairbanks. The table also indicates the material classification for each sample.

Test Hole\ Station	Depth (feet)	Moist Unit Weight (pcf)	Dry Unit Weight (pcf)	Gravimetric Moisture Content (%)	Material Classification
TH13-025\15+00	10 - 11.5	119.5	110.3	8.3	silty Sand
TH13-025	15 - 19.5	123.8	99.6	24.2	silty Sand

Table 16: Southern Main Runway Extension Area Frozen Unit Weight of Soil Test Results.

C. Existing Aircraft Parking Apron, Taxiway and SREB Area Subsurface Findings

The existing aircraft parking apron, taxiway and SREB area was snow covered at the time of our investigation with large snow piles to the west of the apron, and between the runway and apron. The SREB building is located at the southeast corner of the apron, with a cold storage building south of it and two old abandoned buildings and a fuel tank to the north (Figures 10 and 11). To the south of the SREB and apron the original ground slopes moderately to the south. Two test holes were drilled on the existing parking apron and one on the taxiway.



Figure 11: Ambler Airport Existing Aircraft Parking Apron and SREB. View is looking south.

At the time of our investigation, the drill plan was to expand the existing apron and build a new SREB to the north and northeast of the existing apron. This plan is no longer being considered, but our investigation focused in the area to the north of the existing apron. These explorations are discussed in section four of this report under the heading; "not considered new proposed aircraft parking apron and SREB expansion area".

Test holes located on the existing aircraft parking apron and taxiway including the existing SREB area were drilled from 16 to 20 feet in depth. These three test holes encountered the following subsurface conditions:

- Approximately 6 inches thick base course (surface layer) material consisting of frozen silty 0 sand with gravel.
- Thawed material was not encountered. 0
- Frozen material was encountered to depths explored in all three test holes. Permafrost depth 0 could not be determined from any of the test holes.
- Moisture contents ranged from 9.1 to 26.1 percent. Organic contents were slight at 0.5 and 0.6 percent.
- Asbestos testing results from one sample collected at each test hole indicated less than 0.1 0 percent by weight and one asbestos structure for all three holes.

Visible Ice was not encountered in any test holes on the existing parking apron, taxiway and SREB area to depths explored. Frozen material encountered was classified as nonvisible bonded with no excess ice (Nbn), and poorly bonded or friable (Nf). Groundwater or a perched water table was not encountered.

Selected laboratory test results for the existing parking apron, taxiway and SREB area are summarized below in Table 17. The table also indicates frozen material depth, and depth to original ground indicating cut or fill depth from the original main runway profile.

Table 17. Summary of Selected Laboratory Test Results from Test moles at the Existing								
Parking Apron, Taxiway and SREB Area.								
Test Hole and	Depth (feet)	Percent Pagging #200	Frozen Material	Moisture	Cut/Fill			
Siution	(jeel)	Fassing #200	Depth (feet)	Content (%)	(jeel)			
TH13-052\101+00	16		0-16	10.0,9.1	Cut 2			
TH13-053\103+50	20	75.7	0-20	24.9,24.7,12.8,14.2	Fill 3			
TH13-054\103+00	16	77.8	0-16	26.1,20.4	Fill 2			

Table 17: Summary of Selected I above tory Test Desults from Test Holes at the Existing

D. Previous Geotechnical Investigations Subsurface Findings

A summary of previous geotechnical and laboratory test results from investigations preformed in 1973, 1985 and 86 are given below in Tables 18 for the southern portion of the main runway, and Table 19 for the existing aircraft parking apron, taxiway and SREB area. Additional information is presented in Appendix E.

Table 18: Summary of Previous Test Hole Locations, Southern Portion of Main Runway.							
Test Hole and Station	Depth (feet)	Percent Passing #200	Frozen Material	Moisture Content (%)	Cut/Fill (feet)		
		0	Depth (feet)		V /		
TH73-16\19+90	20	65.8	None		At Transition		
TH73-17\24+00	15		None		At Transition		
TH73-18\28+00	15		None		Cut 4		

11 40

Test Hole and Station	Depth (feet)	Percent Passing #200	Frozen Material Depth (feet)	Moisture Content (%)	Cut/Fill (feet)
TH73-19\32+00	15		None		Fill 7.5
TH73-20\36+00	25	79.3	12		Fill 8
TH73-21\40+00	15	81.8	None	13.7	Fill 1.5
TH73-22\44+00	15		7		Fill 2
TH85-1\15+50	11		None		None
TH85-6\22+00	15		11.5		Cut 6
TH85-7\26+00	11	66.0	8.5	17.1	Fill 14.5
TH85-8\30+00	11		9.5		Cut 5.5
TH85-9\34+00	11		9.5		Fill 3.5
TH85-10\38+00	11	60.0	9	13.2	Fill 6.5
TH85-11\42+00	11		9		Cut 1
TH85-12\45+00	11		10		Fill 0.5

 Table 19: Summary of Previous Test Hole Locations, Existing Aircraft Parking Apron,

 Taxiway and SREB.

Test Hole	Depth (feet)	Percent Passing #200	Frozen Material Depth (feet)	Moisture Content (%)	Cut/Fill (feet)
TH85-2\13+00	15	79.0	11.5	13.4	Fill 2
TH85-3\14+50	11		10		Fill 3
TH85-4\14+50	11		None		Fill 2.5
TH85-5\13+00	11		None	19.1	Fill 2
TH73-15\13+00	10		None		Fill 2

3. Existing Airport Access Road and Realignment Area

The existing airport access road is proposed to be realigned around the southern end of the proposed main runway extension, with approximately 850 feet realignment to the northeast of the main runway and south of the existing aircraft parking apron. The existing access road is proposed to be rehabilitated and together with the realignment portion to be resurfaced with surface coarse material or pavement (Figure 12).

The Grizzly Creek Bridge at Grizzly Creek and approximately 2,000 feet south of the main runway is proposed to be replaced with two culverts and the work is being performed under a separate project. R&M Consultants, Inc. in Anchorage, Alaska performed a geotechnical investigation for Grizzly Creek in 2004 with a report dated August 2005 (R&M Consultants, 2005). Our investigation drilled one test hole with a planned second test hole near Grizzly Creek to supplement the report stated above. Due to limited winter access near the bridge and auger refusal in frozen material with gravel, our investigation was limited at Grizzly Creek but results are given for the one shallow test hole.

Test holes drilled for the access road and realignment area were spaced from approximately 250 to 500 feet apart. The test holes on the existing access road were spaced wider to the north of Grizzly Creek as the subsurface material appeared to be consistent (Figure 12). Test Holes were drilled from 3 to 30 feet in depth, and included the following:



Figure 12: Ambler Airport Existing Access Road and Proposed New Realignment, with Test Hole Locations.

- Four test holes (TH13-027 to 030) drilled near the proposed access road realignment, with one test hole TH13-027 moved to the east of the alignment to supplement possible apron expansion.
- Five test holes (TH13-031 and 034, 055 to 057) drilled approximately five feet left or right of the existing access road centerline.
- One test hole (TH13-033) drilled at Grizzly Creek, with limited results due to auger refusal in frozen material with gravel.

A. Existing Access Road Subsurface Findings

The existing access road was snow covered at the time of our investigation with drifting snow at the toe of the embankment. The condition of the road embankment or surface could not be determined. The embankment appeared to be 3 to 6 feet higher than original ground elevation from near the village of Ambler to Grizzly Creek, and none to minor embankment height north of Grizzly Creek as the road passes through approximately 10 foot high moderately sloping cut slopes. A low area was noted near TH13-055 and 034 with a culvert just south of TH13-055.

Test holes located on the existing access road encountered the following subsurface conditions:

- Approximately 1 foot thick base course (surface layer) material consisting of frozen silty sand with gravel.
- Approximately 1 to 5 foot thick embankment material consisting of frozen silt with sand, sandy silt or fine silty sand material. Cobbles were noted at two locations near the surface at TH13-033 and 056.
- Frozen material was encountered in all test holes to depths explored, and therefore permafrost depth could not be determined.
- All test holes were drilled with solid flight augers and soil temperatures in auger cuttings ranged from 27.4 to 32.1 degrees Fahrenheit. These were recorded at test holes TH13-031 and 057.
- Moisture contents ranged from 6.7 to 58.4 percent. The higher moisture contents were encountered in test holes south of Grizzly Creek and lower in test holes north. This also applied to organic contents, with 0.5 and 4.2 percent organics south, and 0.4 and 2.2 percent north.
- Asbestos sample results ranged from 0.2 percent by weight and 56 asbestos structures to less than 0.1 percent by weight and zero structures. The highest asbestos results are given below with test hole number and depth, and the number of asbestos structures found larger than one per sample:
 - 1. TH13-033 at 1 foot in depth and 56 structures and 0.2 percent by weight.
 - 2. TH13-033 at 3 feet in depth and 51 structures and 0.1 percent by weight.
 - 3. TH13-056 at 2 feet in depth and 51 structures and 0.1 percent by weight.
 - 4. TH13-055 at 2.5 feet in depth and 41 structures and 0.2 percent by weight.
 - 5. TH13-057 at 5.5 feet in depth and 6 structures and less than 0.1 percent by weight.

B. Realignment Area Subsurface Findings

The road realignment area was snow covered from 2 to 3 feet in depth, and a trail was plowed for drill rig access. The area slopes gradually from north to south with a few high mounds interrupting drainage, one of these mounds is located at TH13-028. The drainage areas are shallow and wide with TH13-029 located in one drainage area.

Test holes located near the proposed access road realignment area encountered the following subsurface conditions:

- Approximately 1 foot thick organic mat.
- Thawed material was encountered in all but one test hole, and from 12.5 feet to depths explored at 30 feet.
- Moisture contents in thawed material ranged from 7.5 to 26.8 percent. TH13-029 was noted to be wet at 25 feet in depth.

- Frozen material was encountered in all test holes from the surface to 12.5 to 14.5 feet in depth with TH13-028 frozen to the depth explored at 20 feet. Permafrost depth could not be determined in any test holes.
- Test holes drilled with solid flight augers encountered soil temperatures ranging from 21.4 to 38.3 degrees Fahrenheit in auger cutting.
- TH13-028 was drilled with hollow stem augers and one recovered soil core encountered a soil temperature of 31.5 degrees Fahrenheit at 18.5 feet in depth. All test holes indicated increased temperature with depth.
- Moisture contents in frozen material ranged from 3.2 to 18 percent. Organic contents from four samples ranged between 0.3 and 0.5 percent.
- Two asbestos samples collected at TH13-029 from 2.5 and 5.5 feet in depth, indicated less than 0.1 percent by weight and one or zero asbestos structures.

Visible Ice was not encountered in any test holes at the existing access road or proposed realignment area to depths explored. Frozen material encountered was classified as nonvisible bonded with no excess ice (Nbn), and poorly bonded or friable (Nf). Groundwater or a perched water table was not encountered, but wet conditions were noted in TH13-029 at 25 feet.

Selected laboratory test results for the existing access road and realignment area are summarized below in Table 20. The table also indicates frozen material depth, and depth to original ground indicating cut or fill depth from the original access road profile shown in Appendix A and E.

Test Hole and Station	Hole Denth	Percent Passing #200	Frozen Material	Moisture Content (%)	Cut/Fill (feet)
Stution	(feet)	1 ussing 11200	Depth (feet)	Conteni (70)	(jeeij
TH13-027\46+00	20		0-13	18.0,6.2,9.9	None
TH13-028\43+60	20	29.3	0-20	11.4,3.6,5.1,8.2,3.2	None
TH13-029\40+00	30	49.4	0-14.5	6.8,22.6,26.5,22.2	None
TH13-030\36+50	20		0-12.5	12.8,5.1,7.5,8.2	None
TH13-031\31+00	15		0-13	8.9,8.6,9.4,6.7	Fill 3
TH13-033\21+50	4		0-4		Fill 7
TH13-034\15+00	15	71.6	0-15	21.8,20.6,49.0,58.4	At Transition
TH13-055\11+00	15		0-15	21.7,22.8,32.7	Fill 8
TH13-056\19+00	3	28.3	0-3		Fill 5
TH13-057\26+50	15	72.1	0-15	6.9,9.2	Cut 4

Table 20:	Summary of Selected Laboratory	Test Results from	Test Holes at the Existing Access
Road and	Realignment Area.		-

Table 21 below is the laboratory test results for frozen unit weight testing from samples collected at the road realignment area and TH13-028. Results are provided by Shannon and Wilson, Inc. in Fairbanks. The table also indicates the material classification for each sample.

Test Hole\ Station	Sample Depth (feet)	Moist Unit Weight (pcf)	Dry Unit Weight (pcf)	Gravimetric Moisture Content (%)	Material Classification
TH13-028\43+60	10 - 14.5	94.4	87.9	7.5	silty Sand
TH13-028	15 - 19.5	95.8	88.4	8.3	silty Sand

Table 21: Proposed Access Road Realignment Area Frozen Unit Weight of Soil Test Results.

C. Previous Access Road Geotechnical Investigation Subsurface Findings

Previous geotechnical and laboratory test results from the investigation preformed in 1973 are given below in Table 22 for the existing access road. Additional information is shown in Appendix E.

Test Hole	Depth (feet)	Percent Passing #200	Frozen Material	Moisture Content (%)	Cut/Fill (feet)
			Depth (feet)		
TH73-14	15		None		Fill 4
TH73-13	15		None		Fill 1
TH73-12\30+00	15		None		Fill 3
TH73-11\26+00	11	67.6	None		Fill 2
TH13-10\23+50	20		None		Cut 5
TH73-09\22+00	12.5		10		Fill 10
TH73-08\18+00	10		6		Fill 6
TH73-07\14+00	20	55.4	None	10.4	Cut 5
TH73-06\11+00	10	40.9	None	24.5	Fill 8
TH73-05	15	81.5	None	16.6	Cut 3
TH73-04	10		5		Fill 4

Table 22: Summary of Previous Test Holes Drilled at the Existing Airport Access Road.

4. Not Considered Proposed New Aircraft Parking Apron and SREB Expansion Area

At the time of our investigation, the drill plan was to expand the existing parking apron and build a new SREB to the north and northeast of the existing apron and SREB. This plan is no longer being considered. The results of this drilling are presented here.

Test holes drilled included the following:

- Five test holes (TH13-061 to 065) drilled at new SREB area.
- Two test holes (TH13-059 and 060) drilled for new parking apron extension (Figure 13).

All test holes were drilled from 16 to 30 feet in depth. In the new SREB area, TH13-063 was located in a low depression approximately 10 feet in depth and 30 feet in diameter and the remaining test holes located around the edge of the depression. The results of this drilling are presented in Appendix A with laboratory test results presented in Appendix B. SPT blow counts from hollow stem auger test holes drilled at the no longer considered proposed new SREB area are included in the test hole logs presented in Appendix A, Figure 27 and page 57.



Figure 13: Not Considered Proposed New Aircraft Parking Apron and SREB Area, with Test Hole Locations.

Selected laboratory test results for the expansion area are summarized below in Table 23. The table also indicates frozen material depth, and depth to original ground indicating cut or fill depth from the original main runway profile.

Test Hole and Station	Hole Depth (feet)	Percent Passing #200	Frozen Material Depth (feet)	Moisture Content (%)	Cut/Fill (feet)
TH13-059	24	51.3	0-24	7.1,9.5,10.1	None?
TH13-060	16		0-16	6.6,8.6,8.6,9.5	Fill 1-3?
TH13-061	27.5	67.9	0-8.5 and 13.5-27.5	18.3,15.7,6.8,22.7	None
TH13-062	30	64.5	0-8 and 11.5-30	7.6,28.8,18.6	None
TH13-063	30	67.5,48.0	0-4.5	6.9,5.5,7.0,25.2,25.5	None
TH13-064	24	91.2,67.8	0-19 and 21.5-24	8.8,12.3,10.9,12.4	None
TH13-065	30	81.4,59.2	0-10.5	3.6,10.0,13.0	None

Table 23:	Summary	of Selected]	Laboratory J	Cest Results	from Te	st Holes	at the]	Proposed	New
Aircraft Pa	arking Ap	ron Extensio	n and SREB	Area, Not	Consider	ed.			

Selected laboratory test results for the expansion area are summarized below in Table 23. The table also indicates frozen material depth, and depth to original ground indicating cut or fill depth from the original main runway profile.

The officer and the officer and second								
Test Hole and Station	Hole Depth (feet)	Percent Passing #200	Frozen Material Depth (feet)	Moisture Content (%)	Cut/Fill (feet)			
TH13-059	24	51.3	0-24	7.1,9.5,10.1	None?			
TH13-060	16		0-16	6.6,8.6,8.6,9.5	Fill 1-3?			
TH13-061	27.5	67.9	0-8.5 and 13.5-27.5	18.3,15.7,6.8,22.7	None			
TH13-062	30	64.5	0-8 and 11.5-30	7.6,28.8,18.6	None			
TH13-063	30	67.5,48.0	0-4.5	6.9,5.5,7.0,25.2,25.5	None			
TH13-064	24	91.2,67.8	0-19 and 21.5-24	8.8,12.3,10.9,12.4	None			
TH13-065	30	81.4,59.2	0-10.5	3.6,10.0,13.0	None			

 Table 23: Summary of Selected Laboratory Test Results from Test Holes at the Proposed New

 Aircraft Parking Apron Extension and SREB Area, Not Considered.

Table 24 below is the laboratory test results for frozen unit weight testing from samples collected at the expansion area, and provided by Shannon and Wilson, Inc. in Fairbanks. The table also indicates material classification at sample depth.

Test Hole	Sample Depth (feet)	Moist Unit Weight (pcf)	Dry Unit Weight (pcf)	Gravimetric Moisture Content (%)	Material Classification
TH13-061	15 - 16.5	106.2	100.0	6.3	silty Sand
TH13-061	20 - 24.5	124.5	96.4	29.2	silty Sand
TH13-062	10 - 12	100.3	91.6	9.5	silty Sand
TH13-062	15 - 17	106.6	102.2	4.3	silty Sand
TH13-062	20 - 25	93.4	89.3	4.6	silty Sand
TH13-064	5 - 10	102.3	94.4	8.4	Silt
TH13-064	15 - 20	80.7	72.2	11.8	silty Sand
TH13-065	6.5 - 9	107.6	101.7	5.8	silty Sand

 Table 24: Not Considered Proposed New SREB Area Frozen Unit Weight of Soil Test Results.

Expected Physical Site Conditions

Based on variability common in natural environments, climate of the project area and conditions observed in this investigation, anticipate the following physical conditions:

- Expect frozen ground, either seasonally or perennially frozen within the project area at any time of the year.
- Expect perched groundwater on top of frozen layers.
- Expect pumping of silt soils at the bottom of excavations.
- Between those areas not explored expect to encounter areas of massive ice in foundation soils.
- Expect ice-rich soil to be wet and unstable upon thawing.
- Expect thaw bulbs in the vicinity of culverts.
- Expect difficulty handling moist or wet thawed silty soils.

Comments and Recommendations

Our investigation took place during the winter and surface conditions of the runways, apron, taxiway and access road was not observed. According to maintenance staff, the existing main runway gravel surface is in relatively good working condition, with minor thaw rutting and cracking reported during spring break-up. The crosswind runway is reported to have more extensive damage during break-up, which is generally concentrated in the middle of the runway and near the intersection with the main runway, and causes periodic closures.

Comments

- Both the crosswind and main runways currently have a thin surface layer approximately 6 inches thick, and slightly thicker up to approximately 2 feet thick at the southern end of the main runway.
- Two different materials were encountered during drilled:
 - 1. A low drill resistance material that was marginally frozen, poorly bonded and friable. This material was sandy in nature and probably related to the mapped surface dune deposits. The material appeared to be thaw stable, and was generally associated with lower natural moistures.
 - 2. A high drill resistance material that was frozen and well bonded. This material was silty in nature and thaw unstable, and generally associated with higher natural moistures.
- The limits of these two materials are not clearly defined, but in general, sandy material was encountered along the southern portion of the airport. Silty material encountered at the intersection of the two runways and along the crosswind runway.
- Scatter plots of moisture content versus depth indicate moisture contents decrease with depth on the crosswind runway, and increase with depth on the main runway. This may explain the poor condition of the crosswind runway during spring break-up.
- In general, NOA results indicated higher value samples were collected from the main runway and access road locations. NOA values decreased with depth, indicating the surface course material source may locally have NOA values above 0.25 percent. See Appendix C for NOA sample results and the attached chart.
- From as-built drawings and profiles of the main and crosswind runways it is apparent that many cut and fill transitions exist along both runways.
- We encountered thawed wet soil in some test holes at depth, mainly south of the airport and in low areas. Locations included the southern main runway extension area and new access road realignment area. The wet soil conditions could be related to the previous summer and fall high rain events.
- Drilling along the northern portion of the existing access road and north of Grizzly Creek encountered generally sandy material. South of Grizzly Creek test holes encountered predominately silty material underlying the embankment.

Recommendations

North and South Main Runway Extension Areas Paved Surface

- Remove organic mat and organic silts, stockpile for growth media. Estimate this at two (2) feet for volume calculations.
- Drilling at the northern runway extension area and at TH13-001 indicated a possible perched water table. If loose, wet soils are encountered, sub-excavate the wet material and replace with compacted fill.
- Construct embankment to base of non-frost susceptible (NFS) material (NFS material is classified as material with less than 6% passing the #200 sieve) with local materials meeting standard specifications for airport embankments.
- If the embankment below the NFS material is constructed of frost-susceptible material, place a separation geotextile between the two materials.
- Bench new fills into the exiting embankment.
- Construct remaining embankment and structural section as along the main runway.
- Along embankment slopes, ensure edges of the any non-frost susceptible material layers are open to drain; cover with organic material rather than silt.

Gravel Surface

- Remove organic mat and organic silts, stockpile for growth media. Estimate this at two (2) feet for volume calculations.
- Drilling at the northern runway extension area and at TH13-001 indicated a possible perched water table. If wet soil conditions are encountered in foundation material, sub-excavate the wet material and install a woven geotextile fabric.
- Construct embankment to base of non-frost susceptible (NFS) material with local materials meeting standard specifications for airport embankments.
- Place sufficient NFS material to ensure the base of the NFS material, when combined with any base and surface courses, is a total of four (4) feet below the surface. Install separation fabric beneath the NFS material.
- Bench new fills into the exiting embankment.
- We recommend at least 8 inches of surface course.

Existing Main and Crosswind Runways

Paved Surface

• Beneath the main and crosswind runways, safety area, taxiway and apron, excavate and replace the upper embankment with non-frost susceptible material to an effective depth of eight (8) feet. Foam board insulation can be substituted for the NFS embankment material at a rate of 1-inch insulation per foot of NFS material.

- Minimum NFS section thickness is four (4) feet, excluding insulation. The minimum depth to the top of insulation is three (3) feet.
- Install non-woven separation geotextile at the base of the NFS material along the main runway, and reinforcement geotextile along the crosswind runway and under the runway intersection.
- Ensure edges of the NFS layer are open to drain; cover slopes with organic material rather than silt.
- From Station 25+00 to 27+00 drilling encountered organic and high moisture content soils. This corresponds to a fill area indicated from the original main runway profile (Appendix A, Figure 16, Page 46). Sub-excavate this station interval to remove the high moisture and organic soils to a minimum depth of eight (8) feet.
- Construct the embankment to the base of the NFS section with local materials meeting standard specifications for airport embankments.

Gravel Surface

- Either sub-excavate, or raise the grade to ensure the base of the NFS material, when combined with base and surface courses, is a total of four (4) feet below the surface along the taxiway, apron, main and crosswind runways and safety area.
- Install separation geotextile beneath the NFS material.
- We recommend at least eight (8) inches of surface course.

Terrain Obstruction Area and Use of Excavated Materials

- Most of the terrain obstruction drilling encountered marginally frozen, poorly bonded and friable silty sand or sandy silt material.
- This material meets standard specifications for Select Materials Type C, and also airport embankment material.
- One Proctor value indicated optimum moisture content of 14.6%. Samples collected in the area indicated most NM contents in these soils to be at or near optimum moisture.
- Some material may be above optimum moisture requiring draining and drying to achieve optimum compaction.
- Optimum compaction is necessary to avoid differential settlement beneath the runway extension areas.
- NOA contents were all below 0.25%.

Airport Access Road and Realignment

Paved Surface

- Under the re-alignment section, remove organic mat and organic silts, stockpile for growth media. Estimate this at two (2) feet for volume calculations.
- Construct embankment with locally available materials meeting standard specifications for Select Materials, Type C to within forty-two (42) inches of the finished surface. On top of this material place NFS material to the base course layer.
- Install a separation geotextile at the base of the NFS materials.

Gravel Surface

• Remove organic mat and organic silts, stockpile for growth media. Estimate this at two (2) feet for volume calculations.

- Construct embankment with locally available materials meeting standard specifications for Select Materials, Type C.
- Place at least two (2) feet of Select Material, Type B beneath the surface course. If there is the possibility of paving this road in the future, consider increasing the thickness of this layer to forty-two (42) inches.
- Install a separation geotextile at the base of the NFS material.
- We recommend a minimum surface course thickness of eight (8) inches.

Material Sources

Materials source information is not included in this report. A separate report dated April 2013 under project number AKSAS 60851 and titled Ambler Airport Rehabilitation Material Site Report contains information related to all potential material sources for the project.

GEOTECHNICAL REPORT AMBLER SEWAGE LAGOON ROAD STATE PROJECT NUMBER: 61056

Ambler Sewage Lagoon Road

The sewage lagoon was originally built for the village of Ambler in approximately 2005 and located approximately ³/₄ miles southwest, with a cleared and rough access road built as part of the project. The purpose of this project and geotechnical investigation is to rehabilitate the approximately 2,800 liner foot access road, and overlay with surface course material or pavement. Five test holes were drilled along the approximate road alignment with all test holes located on the southeast side of the existing road, and to depths of 10.5 to 15 feet and 400 to 800 feet between holes (Figure 14).



Figure 14: Ambler Sewer Lagoon Road with Test Hole Locations.

The existing lagoon road was snow covered at the time of our investigation and the limits of the road were difficult to determine as well as the location of the sewer line. Mr. Alvin Williams was contacted and he stated the sewer line was located on the northwest side of the road.

Test holes located near the existing lagoon road encountered the following subsurface conditions:

- Approximately 6 inches organic mat, or 1 foot to 1.5 feet thick embankment material consisting of frozen silty sand with gravel.
- Seasonally frozen material was encountered in all test holes to depths ranging from 10.5 to 13 feet, with frozen material encountered throughout TH13-038 to the depth explored at 10.5 feet. Permafrost depth could not be determined in any test holes.
- Moisture contents in frozen material ranged from 16.2 to 39.5 percent, with the highest moisture sampled from TH13-036 and near a peat layer. Organic contents ranged from 0.5 to 4.7 percent.
- All test holes were drilled with solid flight augers and soil temperatures recorded in auger cuttings were 33.2 and 31.7 degrees Fahrenheit in TH13-036 and 035, respectively.
- Thawed material was encountered from 10.5 to depths explored at 15 feet. Moisture contents ranged from 15 to 24.3 percent.
- Asbestos sample results ranged from less than 0.1 percent by weight and 9 asbestos structures to less than 0.1 percent by weight and zero structures. The highest asbestos results are given below with test hole number and depth, and the number of asbestos structures found larger than one per sample:
 - 1. TH13-038 at 3 feet in depth and 9 structures and less than 0.1 percent by weight.
 - 2. TH13-035 at 3 feet in depth and 2 structures and less than 0.1 percent by weight.
 - 3. TH13-042 at 2.5 feet in depth and 2 structures and less than 0.1 percent by weight.

Visible Ice was encountered in TH13-036 from 9 to 10.5 feet in depth, all other test holes did not encountered visible ice to depths explored. Frozen material encountered was classified as nonvisible bonded with no excess ice (Nbn), nonvisible poorly bonded or friable (Nf), and visible ice with inclusions (Vx). See Appendix G for a key to frozen ground classification. Groundwater or perched water was not encountered, but wet soil conditions were noted in TH13-036 and 040 near the bottom of the holes at 11.5 and 13 feet respectively.

Selected laboratory test results for the sewer lagoon road are summarized below in Table 25. The table indicates frozen material depth, and estimates embankment fill depth.

Road.					
Test Hole and Station	Hole Depth (feet)	Percent Passing #200	Frozen Material Depth (feet)	<i>Moisture</i> <i>Content (%)</i>	Fill (feet)
TH13-035	15	84.2,53.0	0-13		1-2?
TH13-036	15	39.1	0-10.5	39.5,24.3	1-3?
TH13-038	10.5		0-10.5	23.6,16.2	None
TH13-040	15		0-11	27.7,23.8,15	None
TH13-042	15		0-12	22.8,16.0	None

 Table 25: Summary of Selected Laboratory Test Results from Test Holes at the Sewer Lagoon

 Road.

Previous explorations were performed in August 29 thru 31, 2002 by Duane Miller and Associates. Five test holes were excavated with a hand auger and shovel to depth of 2 to 4.5 feet (DM&A, 2003).

Expected Physical Site Conditions

Based on variability common in natural environments, climate of the project area and conditions observed in this investigation, anticipate the following physical conditions:

- Expect frozen ground, either seasonally or perennially frozen within the project area at any time of the year.
- Expect perched groundwater on top of frozen layers.
- Expect pumping of silt soils at the bottom of excavations.
- Expect to encounter areas of massive ice in foundation soils.
- Expect ice-rich soil will be wet and unstable upon thawing.
- Expect thaw bulbs in the vicinity of culverts.
- Expect difficulty handling moist or wet thawed silty soils.

Recommendations

The condition of the existing lagoon road could not be determined during this investigation.

These geotechnical recommendations are based on the results of this investigation.

Paving Surface Option

- Remove organic mat and organic silts where encountered, stockpile for growth media. Estimate this at two (2) feet for volume calculations.
- Spread existing embankment.
- Sub-excavate soft or saturated foundation soils when encountered.
- Construct the embankment with materials meeting Select Material, Type C to within forty-two (42) inches of the paved surface.
- Construct to the base course layer with non-frost susceptible (NFS) material.
- Install a separation geotextile at the base of the NFS material.
- Provide positive drainage along the embankment and construct culvert crossings where appropriate.

Gravel Surface Option

- Remove organic mat and organic silts where encountered, stockpile for growth media. Estimate this at two (2) feet for volume calculations.
- Maintain the existing road embankment material.
- Sub-excavate soft or saturated foundation soils when encountered.
- Construct the embankment with materials meeting Select Material, Type C to within two (2) feet of the base course layer.
- Place a minimum of two feet of NFS material.
- Install a separation geotextile at the base of the NFS material.
- We recommend a minimum surface course of eight (8) inches.

Material Sources

Materials source information is not included in this report. A separate report dated April 2013 under project number AKSAS 60851 and titled Ambler Airport Rehabilitation Material Site Report contains information related to all potential material sources for the project.

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APPENDIX A: TEST HOLE LOCATION MAPS, LOGS AND ORIGINAL GROUND PROFILES:

OBSTRUCTION AREA - PAGE 50 -

SOUTH MAIN RUNWAY, TAXIWAY & APRON -PAGES 44, 51, 52

ACCESS RD - PAGE 53, 54, 56

SEWER LAGOON RD - PAGE 56

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NOT CONSIDERED PROPOSED NEW SREB & APRON - PAGE 55



-	FIGURE	15	
-	PAGE	45	-

STATE OF ALASKA DEPARTMENT OF TRANSPORTATION AND PUBLIC FACILITIES ENGINEERING GEOLOGY UNIT

DATA: TW				
DRAWN: JB	AMBLER AIRPORT REHABILITATION			
APPROVED: SM	PROJECT NO. 61303			
DATE: MAY 2013	AMBLER VICINITY MAP			





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\Geo\61303 Ambler Airport\Amblerbase_jb-MAP w TH'S N Main & Xwind 1 Fri, Jun/07/13

Vert

1	TH13-016 N67.10938',	W157.86794		
12	24 FEB	0.0- 0.5 0.5- 1.5	TH13-016 Bn Si SAND w/ Gr (f Gy Sa SILT (fill) Nbn SAMPLE 13-2104 (1.2-1.7) ASBESTOS WT. 0.1%	ill) Nbn
20).0	1.5- 3.0 3.0- 4.5	Bn-Bk SILI w/ Sa (t Bn Sa SILT (fill?) Nbr SAMPLE 13-2105 (3.8-4.2)	ill) Nbn 1
		4.5-12.0	NM 15.4% Tn Si SAND Nf, 31.7 degrees F SAMPLE 13-2106 (5.0-10.0) NM 12.7%, ORG 0.3% 8.0-31.7 degrees F (10.0-15.0) NO SAMPLE RECOVERY 2.0-37 degrees F	
	12	2.0-20.0	12.0- 30.7 degrees F Fn So SILT, Nf cuttings at 31.8 degre SAMPLE 13-2108 (15.0-20.0) ML 66.5% - 200 NP SAMPLE 13-2107 (16.8-17.2) NM 10.8% 19.0- 31.5 degrees F	ees F
	TH13- N67.1	-015 0903'. W157	.86512'	
	6.5 12.5 15.0	0.0 0.5-	TH13-015 0.5 Bn Si SAND w/ 6.5 Bn Sa SILT (fil 2.5-(FILL?) SAMPLE 13-22 (4.5-6.0) NM 17.5% ASBESTOS WT.	/ Gr (fill) Nbn I) Nbn 11 <0.1%
		0.5-1	2.5 III 31 3440 No SAMPLE 13-22 (8.5-9.5) ASBESTOS WT. SM 45.1%-200	
		12.5-1	NM 22.0% 5.0 Bn SILT w/ Sa SAMPLE 13-22 (13.5-15.0) ML 93.0% -200 NM 25.2% 14.5- Auger Re frozen silts	Nbn 13 D, LL—25 NP efusal in tightly
		- FIC	GURE 19 -	
		STATE	OF ALASKA	
0-	DEPAF ENGI	RTMENT AND PUI	OF TRANSPORT BLIC FACILITIES G GEOLOGY (ATION UNIT
ert e	DATA: TW		AMBLER AIRPORT F	REHABILITATION
	APPROVED:	SM	PROJECT NO.	61303
20-	DATE: MAY	2013	NORTH MAIN RUNWAY & C	ROSSWIND RUNWAY



:\Geo\61303 Ambler Airport\Amblerbase_jb-TH'S N Main & Xwind 2 Fri, Jun/07/13 11

Ver

	TH13-007 N67.10707', W15'	7.8538	6'
	27 FEB 27 FEB 2. 2 3 0.0- 5.5 0.5- 8.5	0.5	TH13-007 Bn Si SAND w/ Gr (fill) Nbn Bn Sa SILT (fill) Nbn SAMPLE 13-2148 (0.8-12)
	14.0	5.5	(0.0 1.2) ASBESTOS WT <0.1% Tn Si SAND (fill) Nbn SAMPLE 13-2149 (3.3-3.7) NM 15 5% ORG 0.9%
	5.5- 8.5-	8.5 14.0	4.5- w/ Gr Bn Sa SILT Nbn Bn SILT w/ Sa Nbn SAMPLE 13-2150 (10.8-11.2)
vry	14.0-	-20.0	NM 22.7% 12.0- consistent Bn SILT, Nbn SAMPLE 13-2151 (14.3-14.7) NM 25.6% SAMPLE 13-2152 (15.5-19.5) ORG 0.7% ML 91.0 %-200 LL-22, NP
	TH13-019 N67.10518°, W157.854 19 FEB	485°	
ill) Nbn Ybn 11	0.0- 0.5 0.5- 2.0	5 Br) Br SA (0	TH13—019 n Si SAND w/ Gr (fill) Nbn n—Bk Sa SILT (fill) Nbn MPLE 13—2077 .8—1.2)
) 20 f. NM 25.3%	2.0- 3.0 3.0- 4.0 4.0- 8.5	AS) Tn) Bn 5 Tn SA	BESTOS WI. <0.1% Si SAND (fill) Nf Sa SILT (fill) Nf Si SAND (fill) Nf MPTE 13-2028
,	8.5-11.0	(5 NN 10 SA	0-10.0) 1 3.0%, ORG 0.5% Sa SILT Non 1.0- 23.5 degrees F MPLE 13-2079
-,	11.0-20.0	(1) NM Bn 35 14 so	0.0-14.5) 4 6.5%, ORG 0.5% Si SAND, moist .3 degrees F .0- Nbn, 31.5 degrees F, nd ond silt interloyering,
NM 29.9%		SA (14 NM SA (11 Dry 18	MPLE 13-2080 4.5-15.0) 4.9.4% MPLE 13-2081 5.0-20.0) 7 unit wt. 90.7 pcf, NM 12.1% .0- 31.2 degrees F
	-	FIGL PA	JRE 20 - GE 50 -
0-	STA DEPARTMEN AND I	TE (IT 0. PUBL	OF ALASKA F TRANSPORTATION LIC FACILITIES
rt ee	DATA: TW DRAWN: JB		AMBLER AIRPORT REHABILITATION
20-	APPROVED: SM DATE: MAY 2013	F	PROJECT NO. 61303 NORTH MAIN RUNWAY & CROSSWIND RUNWAY



	TH13-001 N67.11073, W	/157.84919*			
Nbn	20 FEB 0 5.5 5.0 9.0 9.0 1	.0- 1.0	TH13-001 Bn ORG MAT hi C SAMPLE 13-2095 (0.0-5.0) Dry unit wt. 76.9 Bn So SILT Org, 1	Irg pcf, NM Nbn	47.5%
red silt F	20.0	.0- 5.0 .0-20.0	Gy SILT w/ Sa NI 4.5- 31.7 degree Bn Sa SILT SAMPLE 13-2096 (5.0-10.0) NM 29.7%, ORG 0 5.5- moist to we 9.0- Gy Nbe,	bn s F 1.9% t	
id Similor F			30.9 degrees F SAMPLE 13-2097 (10.0-14.5) Dry unit wt. 87.3 SAMPLE 13-2098 (14.5-15.0) NM 38.3%, ORG 1 SAMPLE 13-2099	pcf, NM .0%	37.0%
			(15.0–19.5) Dry unit wt. 86.5 SAMPLE 13–2100 (19.5–20.0) NM 31.4%	pcf, NM	36.2%
		FIGUF – PAG	RE 21 — E 51 —		
0-	ST DEPARTME AND ENGINEE	ATE OI ENT OF PUBLIC ERING	F ALASKA TRANSPORT, C FACILITIES GEOLOGY U	ATION JNIT	
ert t	DATA: TW DRAWN: JB	A	MBLER AIRPORT R	EHABILITA	TION
20-	DATE: MAY 20	13 NOF	RTH MAIN RUNWAY & C	ROSSWIND F	NWAY



V

TH13-011

N67.10776*, W157.85994*

12.5	0.0- 1.0 Bn 0 1.0-20.0 Tn-B SAMP (2.3- ASBE: 3.0- SAMP (4.8- ASBE: 8.5 SAMP (9.8- NM 1 12.5- SAMP (13.2 NM 2 15.0- SAMP (18.8 NM 2	RG MAT hi Org n Si SAND sl Org 2.7) STOS WT. <0.1% Tn Nf LE 13-2226 (5.2) STOS WT. <0.1% 30.8 degrees F LE 13-2227 (10.2) 6.7% - moist to wet LE 13-2228 -13.7) 5.5% - 36.1 degrees F LE 13-2229 -19.2) 9.1%	g, Nbn	
		– FIG – PA	URE 22 - GE 52 -	
⁰⁻	DEF FN	– FIGI – PA STATE ARTMENT O AND PUB	URE 22 – GE 52 – OF ALASKA <i>F TRANSPOR</i> LIC FACILITIE GEOLOGY	TATION S UNIT
fert	DEF EN DATA: TW DRAWN:	- FIG - PA STATE ARTMENT O AND PUB GINEERING	URE 22 – GE 52 – OF ALASKA OF TRANSPOR LIC FACILITIE GEOLOGY AMBLER AIRPORT	TATION S UNIT REHABILITATION
0- fert	DEP EN DATA: TW DRAWN: APPROVED	– FIG – PA STATE STATE CARTMENT O AND PUB GINEERING	URE 22 – GE 52 – OF ALASKA F TRANSPOR LIC FACILITIE GEOLOGY AMBLER AIRPORT PROJECT NO.	TATION S UNIT REHABILITATION 61303



TH13-022 N67.1025	2 1°, W157.8582	9.
ZO FEB		TU13 000
44	00 05	10- C CAND - / C. (CN) Mbs
55 77	0.0- 0.5	Bn Si SAND W/ Gr (IIII) NDN
8.0 44	0.5- 2.0	BN Sa SILI (TII) NON
777=		SAMPLE 13-2117
12.0		(1.2-1.7) NN 6.09
170	20 75	De C CAND - / C (CI) Nhe
17.0	2.0- 5.5	EN DI SAND W/ GE (HII) NON
20.0		(2 2 3 7)
		(J.J-J./)
	16 55	ADDESTOS W1. CU.1%
	3.5- 5.5	SAMDLE 13-2120
		(5 n - 0 5)
		(J.U-3.J)
	55- 80	Ro-Rk SILT w/ So Nho
	0.0-0.0	SAMPLE 13-2119
		(68-72)
		NM 19 7% ORG 1 9%
	80-95	Bn-Tn Si SAND Nf
	010 010	8.5- Silt and organic zones
	9.5-12.0	Bn Sa SILT Nbn,
		30.7 degrees F
		SAMPLE 13-2121
		(9.5-10.0)
		NM 26.9%, ORG 0.8%
		SAMPLE 13-2122
		(10.0-15.0)
		Dry unit wt. 105.8 pcf, NM 23.5%
	12.0-13.0	Bn-Bk SILT w/ Sa Nbn
	13.0-17.0	Bn Sa SILT Nbn
		14.5- 30.6 degrees F, Iron Staining
		SAMPLE 13-2123
		(15.0-19.5)
	170 105	Dry unit wt. 95.7 pct, NM 27.0%
	17.0-10.5	BR SI SAND NDR
	10.3~20.0	195- 304 degrees F
		SAMPLE 13-2124
		(19.5-20.0)
		NM 14.2%
		A MERCY AND A M

IH13-021 N67.10319', W157.8569 27 FEB	9'
2.0	TH13-021 Bn Si SAND w/ Gr (fill) Nbn SAMPLE 13-2160
11.0 20.0	ASBESTOS WT. <0.1% Tn Sa SILT (fill?) Nbn SAMPLE 13-2161 (4.0-9.0)
	ASBESTOS WT. <0.1% ML 57.6%-200 NP 5.0- Nf 7.5- 31.6 degrees F 9.5- Similar
11.0- 20.0	Tn Si SAND Nf 31.4 degrees F SAMPLE 13-2162 (13.8-14.2) NM 6.0%
	16.0- 31.6 degrees F SAMPLE 13-2163 (17.8-18.2) NM 6.4%

TH13-050 N67.10391* 25 FEB	, W157.8568	1'
7775		TH13-050
222	0.0~ 0.5	Bn Si SAND w/ Gr (fill) Nbn
	0.5- 2.0	Bn Sa SILT (fill) Nbn SAMPLE 13-2109 (0.8-1.2)
		NM 7.1%
	2.0- 2.5 2.5- 3.5	Bn. Si SAND w/ Gr (fill) Nbn Bn. So SILT si Org, Nbn SAMPLE 13-2110 (2.8-3.2)
	3.5- 5.5	Tn Si SAND Nf 5.0- 31.8 degrees F SAMPLE 13-2111 (5.0-9.5)
		NM 18.6%
	5.5- 6.5 6.5- 9.0	n So Sill Non Tr Si SAND Non 8.0- Nf
	9.0-10.5	Bn Sa SILT Nbn SAMPLE 13-2112 (9.5-10.0) NM 18.2% SAMPLE 13-2113 (10.0-14.5) Dru woit wt 92.5 ocf NM 30.7%
	10.5-13.5 13.5-20.0	Bn-Bk SILT w/ Sa Nbn Bn Sa SILT Nbn SAMPLE 13-2114 (14.5-15.0) NM 22.5%, ORG 0.5% 15.0- 31.6 degrees F SAMPLE 13-2115 (15.0-19.5)
		Ury unit wt. 95.5 pcf, NM 29.8% 19.0- 31.4 degrees F SAMPLE 13-2116 (19.5-20.0) NM 28.2%

1775		TH13-023
12/5	0.0- 1.0	Bn Si SAND w/ Gr (fill) Nbn
80 11Z	1.0- 8.0	Sa SILT, (fill) Nbn
11.0		SAMPLE 13-2173
		(1.0-6.0) OPC 1.1%
15.0		ML 67.5%-200 NP
20.0 275		SAMPLE 13-2172
20.0		(1.8-2.2)
		ASBESTOS WT. <0.1%
	8.0-11.0	In SL SAND NT SANDLE 13 2174
		(78_82)
		ASBESTOS WT. <0.1%
		8.0- 30.7 degrees F, Consistent
	11.0-15.0	Bn-Tn So SILT sl Org, Nbn
		SAMPLE 13-2175
		(11.8-12.2) NN 25.09
	15.0-20.0	To Si SAND NE
	1010 2010	16.5- 31.7 degrees F
		SAMPLE 13-2176
		(18.3-18.7)
		MIL 10 59

TH13-020 N67.10460', V 27 FEB	W157.8557	0,
2.5	0.0- 0.5	TH13-020 Bn Si SAND w/ Gr (fill) Nbn
	0.5- 2.5	Bn-Bk Sa SILT (fill) Nbn
9.0 LLA 2	2.5- 3.5	Tn Si SAND (fill) Nbn
12.5	8.5- 9.0	Bn SILT w/ So (fill?) Nbn SAMPLE 13-2156
20.0		(3.8-4.2) NM 19.2%, ORG 1.3% SAMPLE 13-2157
		(5.0-9.0) ORG 2.0%,
		ASBESTOS WT. <0.1% ML 78.9%-200 LL-22 NP 6.5- Consistent 8.5- Oro, Wood Chips
9	.0-12.5	Tn Si SAND Nbn 10.5- Bn
12	5-20.0	Bn-Gr SILT w/Sa Nbn SAMPLE 13-2158
		(13.8-14.2)
		NM 27.8%
		SAMPLE 13-2159
		(17.3-17.7) NM 27.5%

5.5

9.0

13.5

20.0



- FIGURE 24 -







i.e

TH13-061 N67.10137 16 FFB	', W157.8562	2'		
8.5 8.0	0.0- 1.0 1.0- 8.0	TH13-061 Bn ORG MAT h Bn So SILT Ori SAMPLE 13-20	i Org g, Nbn 56	
13.5 18.5 23.0 25.5 27.5	8.0-18.5	(1.8-2.2) NM 18.3%, OR(SAMPLE 13-200 (4.5-8.0) ORG 1.2% ML 67.9%-200 Th Si Sand, Nt 8.5- Sampler SAMPLE 13-200 (10.0-12.0) BI NM 15.7% 12.0- 32.4 de SAMPLE 13-20	S 0.7% 57 n plugged off, moist 58 .0W COUNTS: 3, 5, 4, 4 grees F 59	
	18.5-23.0	(15.0-16.5) Bl Dry unit wt. 10 16.0-31.3 de SAMPLE 13-200 (16.5-17.0) NM 6.8% Bn So SILT Nf SAMPLE 13-20 (20.0-24.5) Dry unit wt. 96 21.0- Interlaye	OW COUNTS: 3, 5, 6, 5 10.0 pcf, NM 6.3% grees F, NF 60 61 64 pcf, NM 29.2% red silt and sand	
bn	23.0-25.5	22.5- 31.8 de Bn Si SAND Nf SAMPLE 13-20	grees F grees F 62	
) NP, ORG 0.5%	25.5-27.5	(24.5-25.0) NM 22.7% Bn Sa SILT Nbr 27.0- Refusal	n in tightly frozen silts	
ó degrees F				
NT: 10, 13, 11, 8				
f, NM 5.8%				
, moist				
UNTS: 3, 5, 6, 6				
dium dense				
NP				
UNTS: 3, 4, 4, 4				
UNTS: 3, 4, 4, 7		- FIC - P/	AGE 57 -	
0	. DE	STATE	OF ALASKA OF TRANSPORTATION	
0-	EI	VGINEERIN	G GEOLOGY UNIT	
ert e	DATA: T	W	AMBLER AIRPORT REHABILITATION	1
- Stee	DRAWN:	JB D: SM	PROJECT NO 61303	
20-	DATE:	MAY 2013	NOT CONSIDERED PROPOSED	
	Contraction of the	1000 0000 0000	NEW SKEB & APRON	_



20-

N67.08265', W157.87454'

0.0- 1.0 Bn Si SAND w/ Gr (fill) Nbn 1.0- 4.0 Gy SILT w/Sa Nbn SAMPLE 13-2281 (1.5 - 4.5)ASBESTOS WT. <0.1% ML 84.2%-200 LL-20 NP 4.0-15.0 Bn Sa SILT Nbn 6.0 Nf (6.0 - 9.0)

TH13-035

SAMPLE 13-2282 ML 53.0%-200 NP 7.5- 31.7 degrees F 9.0- Consistent 13.0- 32.6 degrees F, moist

- FIGURE 28 -- PAGE 58 -STATE OF ALASKA DEPARTMENT OF TRANSPORTATION AND PUBLIC FACILITIES ENGINEERING GEOLOGY UNIT AMBLER SEWAGE LAGOON ROAD

DATE: MAY 2013

PROJECT NO.

61056

SEWER LAGOON ROAD

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APPENDIX B: LABORTORY TEST RESULTS:

PROJECT N PROJECT N	IAME: II IMBER:	Ambler Airpo	Ambler Airport Rehibilation							
AKSAS NUN SAMPLED B MATERIAL S	<i>IBER:</i> }Y: SOURCE:	61303 T. Weiss CENTERLIN	JE, NORTHER	N MAIN RUN	NAY					
TEST HOLE DEPTH (feet STATION OFFSET LAB NUMBE DATE SAMF	NUMBER ') ER PLED	TH13-001 5.0-10.0 58+00 15L 13-2096 20-Feb-13	TH13-001 14.5-15.0 58+00 15L 13-2098 20-Feb-13	TH13-001 19.5-20.0 58+00 15L 13-2100 20-Feb-13	TH13-002 2.8-3.2 55+50 45R 13-2191 28-Feb-13	TH13-002 8.8-9.2 55+50 45R 13-2192 28-Feb-13	TH13-002 11.8-12.2 55+50 45R 13-2193 28-Feb-13	TH13-002 18.3-18.7 55+50 45R 13-2194 28-Feb-13		
% Passing Gravel	3" 2" 1.5" 1.0" 0.75" 0.5" 0.375" #4									
Sand	#8 #10 #16 #30 #40 #50 #60 #80 #100									
Silt/Clay	#200									
Hydro	0.02 0.005 0.002 0.001									
LIQUID LIMIT PLASTIC IND USCS CLASS	-)EX SIFICATION									
USCS SOIL E	DESCRIPTION	(SaSi)	(SaSi)	(SaSi)	(SiSa)	(SiSa)	(SiSa)	(SiSa)		
NATURAL M ORGANICS SP. GR. (FINI SP. GR. (COA MAX. DRY DE OPTIMUM M L.A. ABRASIC DEGRAD. FA SODIUM SUL SODIUM SUL NORDIC ABF	DISTURE E) ARSE) ENSITY OISTURE DN IGTOR .F. (CRSE) .F. (FINE) RASION	29.7 0.9	38.4 1.0	31.4	11.5	6.8	9.3	11.5		
REMARKS								- · · ·		
		1								
GENERAL CO	OMMENTS	Gradation is based ¹ Organic content (Soil descriptions USCS Soil Descri	t on material passing determination is bas shown in parenthes iption Abbreviations	g the 3" sieve, accor sed on the results of es are based on field s: WG = Well-grade	ding to Alaska Test the ATM T-6 test m (determinations.) ed; PG = Poorly-gra	Method T-7. nethod. aded; E = Elastic; I	L = Lean; F = Fat			

PROJECT N PROJECT N AKSAS NUN SAMPLED E MATERIAL \$	IAME: IUMBER: IBER: BER: 3Y: SOURCE:	Ambler Airpo 61303 T. Weiss CENTERLIN	ort Rehibilation ↓E, NORTHER	N MAIN RUN	NAY			
TEST HOLE DEPTH (feet STATION OFFSET LAB NUMBE DATE SAMF	NUMBER !) ER PLED	TH13-004 6.3-6.7 50+50 25L 13-2022 13-Feb-13	TH13-004 9.8-10.3 50+50 25L 13-2023 13-Feb-13	TH13-004 14.8-15.2 50+50 25L 13-2024 13-Feb-13	TH13-003 3.2-3.7 52+50 15L 13-2196 28-Feb-13	TH13-003 2.0-7.0 52+50 15L 13-2197 28-Feb-13	TH13-003 8.8-9.2 52+50 15L 13-2198 28-Feb-13	TH13-003 14.8-15.2 52+50 15L 13-2199 28-Feb-13
% Passing Gravel	3" 2" 1.5" 1.0" 0.75" 0.5" 0.375" #4							
Sand	#8 #10 #16 #30 #40 #50 #60 #80 #100					100 99 98 97 95		
Silt/Clay	#200 0.02 0.005					69.1		·
Hydro	0.002 0.001							
LIQUID LIMIT PLASTIC INE USCS CLASS	- DEX SIFICATION					NV NP ML		
USCS SOIL E	DESCRIPTION	(SaSi)	(SiSa)	(SiSa)	SaSi	SaSi	(SiSa)	(SiSa)
NATURAL M ORGANICS SP. GR. (FIN, SP. GR. (CO) MAX. DRY D OPTIMUM M L.A. ABRASIC DEGRAD. FA SODIUM SUL SODIUM SUL NORDIC ABF	DISTURE E) ARSE) ENSITY OISTURE DN ICTOR LF. (CRSE) LF. (CRSE) LF. (FINE) RASION	12.8 0.8	11.4	17.5 0.6	8.3 0.6		8.4	14.1 1.7
REMARKS								
GENERAL CO	<i>OMMENTS</i>	Gradation is based ¹ Organic content (Soil descriptions USCS Soil Descri	t on material passing determination is bas shown in parenthes iption Abbreviations	g the 3" sieve, accor sed on the results of es are based on field s: WG = Well-grade	ding to Alaska Test the ATM T-6 test n determinations.) ed; PG = Poorly-gra	Method T-7. nethod. aded; E = Elastic; :	L = Lean; F = Fat	

Ambler Airport Rehibilation

PROJECT NAME:Ambler Aliport PPROJECT NUMBER:61303AKSAS NUMBER:T. WeissSAMPLED BY:CENTERLINE,MATERIAL SOURCE:CENTERLINE,

T. Weiss CENTERLINE, NORTHERN MAIN RUNWAY

TEST HOLE NUMBER DEPTH (feet) STATION OFFSET LAB NUMBER DATE SAMPLED	TH13-004 15.0-20.0 50+50 25L 13-2025 13-Feb-13	TH13-004 17.2-17.7 50+50 25L 13-2026 13-Feb-13	TH13-005 1.3-1.7 48+00 5R 13-2088 20-Feb-13	TH13-005 2.0-6.5 48+00 5R 13-2090 20-Feb-13	TH13-005 5.0-10.0 48+00 5R 13-2091 20-Feb-13	TH13-005 12.8-13.2 48+00 5R 13-2092 20-Feb-13	TH13-005 10.0-14.0 48+00 5R 13-2093 20-Feb-13
% Passing 3" 2" 1.5" Gravel 0.75" 0.5" 0.375" #4							
#8 #10 #16 #30 Sand #40 #50 #60 #80 #100	100 99 99 96 96 93			100 99 99 98 98 98 97 96	99 99 98 97 97 96 96 96 94 93		100 99 99 98 96
Silt/Clay #200	46.6			76.4	75.5		72.7
0.02 0.005 0.002 0.001							
LIQUID LIMIT PLASTIC INDEX USCS CLASSIFICATION	NV NP SM			20 NP ML	NV NP ML		NV NP ML
USCS SOIL DESCRIPTION	SiSa	SiSa	(SaSi)	Si w/Sa	Si w/Sa	Si w/Sa	Si w/Sa
NATURAL MOISTURE ORGANICS SP. GR. (FINE) SP. GR. (COARSE) MAX. DRY DENSITY OPTIMUM MOISTURE L.A. ABRASION DEGRAD. FACTOR SODIUM SULF. (CRSE) SODIUM SULF. (FINE) NORDIC ABRASION		20.9 1.3	20.4		3.0	21.0 0.7	
REMARKS					sl Org¹		
GENERAL COMMENTS	Gradation is base ¹ Organic content (Soil descriptions USCS Soil Descr	d on material passi t determination is ba s shown in parenthe ription Abbreviation	ng the 3" sieve, acco used on the results of ses are based on fiel s: WG = Well-grad	rding to Alaska Tes f the ATM T-6 test n d determinations.) ed; PG = Poorly-gr	t Method T-7. method. aded; E = Elastic;	L = Lean; F = Fat	

PROJECT N PROJECT N AKSAS NUN SAMPLED E MATERIAL S	IAME: IUMBER: MBER: 3Y: SOURCE:	Ambler Airpo 61303 T. Weiss CENTERLIN	et, NORTHER	N MAIN RUNV	VAY and CRO	SSWIND RUN	WAY	
TEST HOLE DEPTH (fee STATION OFFSET LAB NUMBE DATE SAMF	NUMBER t) ER PLED	TH13-006 4.3-4.7 43+50 12R 13-2033 13-Feb-13	TH13-006 5.0-8.0 43+50 12R 13-2034 13-Feb-13	TH13-006 10.8-11.2 43+50 12R 13-2035 13-Feb-13	TH13-005 14.0-14.5 48+00 5R 13-2094 20-Feb-13	TH13-007 3.3-3.7 507+00 15R 13-2149 27-Feb-13	TH13-007 10.8-11.2 507+00 15R 13-2150 27-Feb-13	TH13-007 14.3-14.7 507+00 15R 13-2151 27-Feb-13
% Passing Gravel	3" 2" 1.5" 1.0" 0.75" 0.5" 0.375" #4							
Sand	#8 #10 #16 #30 #40 #50 #60 #80 #100		100 99 98 98 98 97 97					
Silt/Clay	#200		85.6					
Hydro	0.005 0.002 0.001							
LIQUID LIMI PLASTIC INI USCS CLAS	T DEX SIFICATION		23 NP ML	17 NP				
USCS SOIL	DESCRIPTION	(Si w/Sa)	Si	(Si w/Sa)	(SaSi)	(SiSa)	(Si w/Sa)	(Si w/Sa)
NATURAL M ORGANICS SP. GR. (FIN SP. GR. (CO MAX. DRY E OPTIMUM M L.A. ABRASI DEGRAD. FJ SODIUM SU NORDIC AB	IOISTURE IE) WARSE) DENSITY IOISTURE ON ACTOR LF. (CRSE) LF. (FINE) RASION	22.6 1.3	1.3	25.3	22.0	15.5 0.9	22.7	25.6
REMARKS								
GENERAL C	OMMENTS	Gradation is base ¹ Organic content (Soil descriptions USCS Soil Descr	d on material passir determination is ba shown in parenthes iption Abbreviation	l g the 3" sieve, acco sed on the results of ses are based on field s: WG = Well-grad	I rding to Alaska Tes f the ATM T-6 test f d determinations.) ed; PG = Poorly-gr	I t Method T-7. method. raded; E ≈ Elastic;	L = Lean; F = Fat	1

Ambler Airport Rehibilation

61303

PROJECT NAME: PROJECT NUMBER: AKSAS NUMBER: SAMPLED BY: MATERIAL SOURCE:

T. Weiss CENTERLINE, NORTHERN MAIN RUNWAY and CROSSWIND RUNWAY and OBSTRUCTION AREA

TEST HOLE DEPTH (fee STATION OFFSET LAB NUMBI DATE SAMI	E NUMBER ht) ER PLED	TH13-008 3.3-3.7 40+00 10L 13-2036 13-Feb-13	TH13-008 10.3-10.7 40+00 10L 13-2038 13-Feb-13	TH13-008 12.8-13.2 40+00 10L 13-2039 13-Feb-13	TH13-007 15.5-19.5 507+00 15R 13-2152 27-Feb-13	TH13-009 4.8-5.2 40+50 310L 13-2215 1-Mar-13	TH13-009 9.0-15.0 40+50 310L 13-2217 1-Mar-13	TH13-009 12.8-13.2 40+50 310L 13-2218 1-Mar-13
% Passing	3" 2"							
Gravel	1.5" 1.0" 0.75" 0.5" 0.375"							
	#4 #8							
	#10 #16							
Sand	#30							
Curra	#40 #50						100	
	#60 #80						99	
Silt/Clav	#100 #200				100 91.0		98 85.0	
Siluciay	0.02							
Hydro	0.005 0.002 0.001							
					22 ND		NV NP	
USCS CLAS	SIFICATION				ML		ML	
USCS SOIL	DESCRIPTION	(SaSi)	(SaSi)	(Si w/Sa)	Si	(SiSa)	Si	(SiSa)
NATURAL N	IOISTURE	25.1	24.6	28.0	0.7	11.7 1.0		8.9
SP. GR. (FI	VE)		0.5		0.7	1.0		
SP. GR. (CC MAX. DRY L	DARSE) DENSITY							
OPTIMUM N	IOISTURE							
DEGRAD. F.	ACTOR							
SODIUM SU	ILF. (CRSE) ILF. (FINE)							
NORDIC AB	RASION							
REMARKS								
GENERAL (COMMENTS	Gradation is base	d on material passin	g the 3" sieve, acco	rding to Alaska Test	t Method T-7.	l	
		¹ Organic content (Soil descriptions	determination is ba	sed on the results of	the ATM T-6 test and the test and the terminations (nethod.		
		USCS Soil Descr	iption Abbreviation	s: WG = Well-grad	ed; PG = Poorly-gr	aded; E = Elastic;	L = Lean; F = Fat	

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PROJECT NAME:Ambler Airport RehibilationPROJECT NUMBER:61303AKSAS NUMBER:T. WeissSAMPLED BY:CENTERLINE, OBSTRUCTION AREAMATERIAL SOURCE:CENTERLINE, OBSTRUCTION AREA

TEST HOLE NUMBER DEPTH (feet) STATION OFFSET LAB NUMBER DATE SAMPLED	TH13-012 2.8-3.2 515+00 55R 13-2201 28-Feb-13	TH13-010 1.5-10.0 512+50 310L 13-2221 1-Mar-13	TH13-010 6.8-7.2 512+50 310L 13-2222 1-Mar-13	TH13-010 10.0-15.0 512+50 310L 13-2223 1-Mar-13	TH13-011 9.8-10.2 516+00 80L 13-2227 1-Mar-13	TH13-011 13.2-13.7 516+00 80L 13-2228 1-Mar-13	TH13-011 18.8-19.2 516+00 80L 13-2229 1-Mar-13
% Passing 3" 2"							
1.5" <i>Gravel</i> 1.0" 0.75" 0.5" 0.375" #4							
#8 #10 #16 #30 Sand #40		100		100			
#50 #60 #80 #100		99 99 98 97		99 99 96 94			
Silt/Clay #200		50.2		45.3			
0.02 0.005 0.002 0.001							
LIQUID LIMIT PLASTIC INDEX USCS CLASSIFICATION	,	NV NP ML		NV NP SM			
USCS SOIL DESCRIPTIO	ON (Si w/Sa)	SaSi	SaSi	SiSa	(SiSa)	(SiSa)	(SiSa)
NATURAL MOISTURE ORGANICS SP. GR. (FINE)	23.5 0.8	2.66	7.5	2 71	16.7	25.5	29.1
SP. GR. (COARSE) MAX. DRY DENSITY OPTIMUM MOISTURE L.A. ABRASION DEGRAD. FACTOR SODIUM SULF. (CRSE) SODIUM SULF. (FINE) NORDIC ABRASION		2.00		102.0			
REMARKS		T-99 was used		T-99 was used			
GENERAL COMMENTS	Gradation is bas Organic conten (Soil description USCS Soil Desc	ed on material passi at determination is bi s shown in parenthe ription Abbreviatior	ng the 3" sieve, acco ased on the results o ses are based on fiel as: WG = Well-grad	, ording to Alaska Tes f the ATM T-6 test d determinations.) led; PG = Poorly-gr	at Method T-7. method. raded; E = Elastic;	L = Lean; F = Fat	

COMPACTION REPORT

Project: Ambler Airport Rehabilitation

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Lab Number: 13-2221



PROJECT N PROJECT N AKSAS NUM SAMPLED B MATERIAL S	AME: UMBER: IBER: IY: SOURCE:	Ambler Airpo 61303 T. Weiss CENTERLIN	ort Rehibilation	ND RUNWAY	and OBSTRUC	CTION AREA		
TEST HOLE DEPTH (feet STATION OFFSET LAB NUMBE DATE SAMP	NUMBER)) ER PLED	TH13-013 1.8-2.2 518+50 15L 13-2125 25-Feb-13	TH13-013 5.0-9.5 518+50 15L 13-2126 25-Feb-13	TH13-013 9.5-10.0 518+50 15L 13-2127 25-Feb-13	TH13-012 7.3-7.7 515+00 55R 13-2203 28-Feb-13	TH13-012 8.8-9.2 515+00 55R 13-2204 28-Feb-13	TH13-012 13.3-13.7 515+00 55R 13-2205 28-Feb-13	TH13-014 2.3-2.7 521+50 52L 13-2206 28-Feb-13
% Passing Gravel	3" 2" 1.5" 1.0" 0.75" 0.5" 0.375" #4							
Sand	#8 #10 #16 #30 #40 #50 #60 #80 #100		100 99 99					
Silt/Clay	#200		90.5					
Hydro	0.02 0.005 0.002 0.001							
LIQUID LIMIT PLASTIC INE USCS CLASS	T DEX SIFICATION		NV NP ML					
USCS SOIL I	DESCRIPTION	(Si w/Sa)	(Si w/Sa)	(Si w/Sa)	(Si w/Sa)	(Si w/Sa)	(SiSa)	(Si w/Sa)
NATURAL M ORGANICS SP. GR. (FIN SP. GR. (CO, MAX. DRY D OPTIMUM M L.A. ABRASM DEGRAD. FA SODIUM SUI NORDIC ABF	OISTURE ARSE) ENSITY OISTURE ON ACTOR LF. (CRSE) LF. (FINE) RASION	26.6	0.7	23.1 0.6	14.2 0.9	15.0	6.5	32.5 1.0
REMARKS								
GENERAL C	OMMENTS	Gradation is base ¹ Organic content (Soil descriptions USCS Soil Descr	d on material passi determination is ba shown in parenthe: iption Abbreviation	ng the 3" sieve, acco ased on the results of ses are based on fiel as: WG = Well-grad	rding to Alaska Tes f the ATM T-6 test f d determinations.) led; PG = Poorly-gr	, t Method T-7. nethod. aded; E = Elastic;	L = Lean; F = Fat	

PROJECT NAME:	Ambler Airport Rehibilation
PROJECT NUMBER: AKSAS NUMBER: SAMPLED BY: MATERIAL SOURCE:	61303 T. Weiss CENTERLINE, CROSSWIND RUNWAY

DEPTH (fee STATION OFFSET LAB NUMBE DATE SAME	: NUMBER t) ER PI ED	TH13-015 4.5-6.0 525+50 34R 12-2211 28-Feb-13	TH13-016 3.8-4.2 529+00 CL 13-2105 24-Eeb-13	TH13-014 2.5-6.5 521+50 52L 13-2208 28-Feb-13	TH13-014 8.6-9.5 521+50 52L 13-2209 28-Feb-13	TH13-014 13.0-14.5 521+50 52L 13-2210 28.Feb-13	TH13-015 8.5-9.5 525+50 34R 13-2212 28-Feb-13	TH13-015 13.5-15.0 525+50 34R 1 3-2213 28-Eeb-13
% Passing Gravel	3" 2" 1.5" 1.0" 0.75" 0.5"	201 60-13	241 60-13	201 60-13	201 60-13	201 60-13	201 60-13	20-1 - 13
	0.375" 							
Sand	#10 #16 #30 #40 #50 #60 #80 #100			100 99 99	100 99 99	100 99 99 99 99 98 97	100 89 84 73 68	99 99 99 99 99 99 99 99
Silt/Clay	#200			92.3	91.6	79.4	45.1	93.0
Hydro	0.02 0.005 0.002 0.001							
LIQUID LIMI PLASTIC INE USCS CLAS	T DEX SIFICATION			NV NP ML	NV NP ML	29 NP ML	24 NP SM	25 NP ML
USCS SOIL I	DESCRIPTION	(SaSi)	(SaSi)	Si	Si	Si w/Sa	SiSa	Si
NATURAL M ORGANICS SP. GR. (CO. MAX. DRY D OPTIMUM M L.A. ABRASIM DEGRAD. FA SODIUM SUI SODIUM SUI	OISTURE E) ARSE) ENSITY OISTURE ON ACTOR LF. (CRSE) LF. (CRSE) LF. (FINE) RASION	17.5	15.4	1.2	17.6 0.9	28.7 4.9	22.0	25.3
REMARKS						sl Org¹		
GENERAL C	OMMENTS	Gradation is based ¹ Organic content (Soil descriptions USCS Soil Descri	d on material passing determination is bas shown in parenthes ption Abbreviations	g the 3" sieve, accor sed on the results of es are based on field :: WG = Well-grade	ding to Alaska Test the ATM T-6 test m determinations.) d; PG = Poorly-gra	Method T-7. nethod. ided; E = Elastic; I	. = Lean; F = Fat	

PROJECT N PROJECT N AKSAS NUN SAMPLED B MATERIAL S	AME: IUMBER: IBER: IY: SOURCE:	Ambler Airpo 61303 T. Weiss CENTERLIN	Ambler Airport Rehibilation 61303 T. Weiss CENTERLINE, MAIN AND CROSSWIND RUNWAY, OBSTRUCTION AREA					
TEST HOLE DEPTH (feet STATION OFFSET LAB NUMBE DATE SAMF	NUMBER () ER PLED	TH13-019 5.0-10.0 36+00 52R 13-2078 19-Feb-13	TH13-016 5.0-10.0 529+00 CL 13-2106 24-Feb-13	TH13-016 16.8-17.2 529+00 CL 13-2107 24-Feb-13	TH13-016 15.0-20.0 529+00 CL 13-2108 24-Feb-13	TH13-017 4.8-5.2 38+00 550L 13-2238 1-Mar-13	TH13-017 12.8-13.2 38+00 550L 1 3-2240 1-Mar-13	TH13-018 1.0-7.0 35+50 300L 13-2242 1-Mar-13
% Passing Gravel	3" 2" 1.5" 1.0" 0.75" 0.5" 0.375" #4							
Sand	#8 #10 #16 #30 #40 #50 #60 #80 #100				100 99 97			100 99 99 97 96
Silt/Clay	#200				66.5			62.9
Hydro	0.02 0.005 0.002 0.001							
LIQUID LIMI PLASTIC INI USCS CLAS	T DEX SIFICATION				NV NP ML			NV NP ML
USCS SOIL	DESCRIPTION	(SaSi)		SaSi	SaSi	(SiSa)	(SiSa)	SaSi
NATURAL M ORGANICS SP. GR. (FIN SP. GR. (CO MAX. DRY D OPTIMUM M L.A. ABRASI DEGRAD. FA SODIUM SU SODIUM SU NORDIC ABI	OISTURE ARSE) ENSITY OISTURE ON ACTOR LF. (CRSE) LF. (FINE) RASION	13.0 0.5	12.7 0.3	10.8		10.9 0.2	14.9	1.1
REMARKS								
GENERAL C	OMMENTS	Gradation is base ¹ Organic content (Soil descriptions USCS Soil Descr	d on material passir determination is ba s shown in parenthes iption Abbreviation	ng the 3" sieve, acco sed on the results of ses are based on fiel s: WG = Well-grad	rding to Alaska Tes f the ATM T-6 test t d determinations.) ed; PG = Poorly-gr	t Method T-7. nethod. aded; E = Elastic;	L = Lean; F = Fat	

Ambler Airport Rehibilation

PROJECT NAME:	Ambler Airport Rehibilation
PROJECT NUMBER: AKSAS NUMBER: SAMPLED BY:	61303 T. Weiss
MATERIAL SOURCE:	CENTERLINE, MAIN RONWAT

TEST HOLE NUMBER DEPTH (feet) STATION	TH13-019 10.0-14.5 36+00	TH13-019 14.5-15.0 36+00	TH13-020 3.8-4.2 33+50	TH13-020 5.0-9.0 33+50	TH13-020 13.8-14.2 33+50	TH13-020 17.3-17.7 33+50	TH13-021 4.0-9.0 28+00
OFFSET	52R	52R	8R	8R	8R	8R	15R
LAB NUMBER	13-2079	13-2080	13-2156	13-2157	13-2158	13-2159	13-2161
% Passing 3"	19-rep-13	19-Feb-13	27-Feb-13	27-1 60-13	27-1 60-13	27-1 60-10	27-1 00-10
2" 1.5" Gravel 1.0" 0.75" 0.5" 0.375" #4							
#8							99
#10				100			99
#16				99			99
Sand #40				98			98
#50				97			97
#60				97			97
#80				95			95
#100 Silt/Clov #200				78.9			57.0
0.02			1	10.0			0110
Hydro 0.005 0.002 0.001							
LIQUID LIMIT				22			NV
PLASTIC INDEX				NP			
USCS CLASSIFICATION							
USCS SOIL DESCRIPTION	(SiSa)	(SiSa)	(SaSi)	Si w/Sa	(Si w/Sa)	(Si w/Sa)	SaSi
NATURAL MOISTURE	6.5	9.4	19.2		27.8	27.5	
ORGANICS	0.5		1.3	2.0			
SP. GR. (COARSE)							
MAX. DRY DENSITY							
OPTIMUM MOISTURE							
L.A. ABRASION							
SODIUM SULF. (CRSE)							
SODIUM SULF. (FINE)							
NORDIC ABRASION							
REMARKS							
			<u> </u>	1]	
GENERAL COMMENTS	Gradation is base	ed on material passir t determination is ba	ig the 3" sieve, acco used on the results of	rding to Alaska Tes Tthe ATM T-6 test i	t Method 1-7. nethod.		
	(Soil descriptions shown in parentheses are based on field determinations.)						
	USCS Soil Descr	ription Abbreviation	s: WG = Well-grad	ed; PG = Poorly-gr	aded; E = Elastic;	L = Lean; F = Fat	

PROJECT NAME:	Ambler Airport Rehibilation			
PROJECT NUMBER: AKSAS NUMBER: SAMPLED BY: MATERIAL SOURCE:	61303 T. Weiss CENTERLINE, MAIN RUNWAY			

TEST HOLE DEPTH (fee STATION OFFSET LAB NUMBL	E NUMBER t) ER	TH13-022 1.2-1.7 25+00 30L 13-2117	TH13-022 6.8-7.2 25+00 30L 13-2119	TH13-022 5.0-9.5 25+00 30L 13-2120	TH13-022 9.5-10.0 25+00 30L 13-2121	TH13-022 19.5-20.0 25+00 30L 13-2124	TH13-021 13.8-14.2 28+00 15R 13-2162	TH13-021 17.8-18.2 28+00 15R 13-2163
DATE SAM	PLED	25-Feb-13	25-Feb-13	25-Feb-13	25-Feb-13	25-Feb-13	27-Feb-13	27-Feb-13
% Passing Gravel	3" 2" 1.5" 1.0" 0.75" 0.5" 0.375" #4							
Sand	#8 #10 #16 #30 #40 #50 #60 #80 #100							
Silt/Clay	#200							
Hydro	0.02 0.005 0.002 0.001							
LIQUID LIMI PLASTIC INE USCS CLAS	T DEX SIFICATION							
USCS SOIL I	DESCRIPTION	(SaSi)	(Si w/Sa)	(SiSa)	(SaSi)	(SaSi)	(SiSa)	(SiSa)
NATURAL M ORGANICS SP. GR. (FIN SP. GR. (CO. MAX. DRY D OPTIMUM M L.A. ABRASI DEGRAD. FA SODIUM SU SODIUM SU NORDIC ABF	OISTURE ARSE) ENSITY OISTURE ON ACTOR LF. (CRSE) LF. (CINE) RASION	6.0	19.7 1.9	41.1	26.9 0.8	14.2	6.0	6.4
REMARKS								
GENERAL C	OMMENTS	Gradation is based ¹ Organic content (Soil descriptions USCS Soil Descri	t on material passing determination is bas shown in parenthese ption Abbreviations	g the 3" sieve, accor ed on the results of es are based on field : WG = Well-grade	ding to Alaska Test the ATM T-6 test m determinations.) d; PG = Poorly-gra	Method T-7. hethod. ded; E = Elastic; L	. = Lean; F = Fat	
PROJECT NAME:	Ambler Airport Rehibilation							
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PROJECT NUMBER: AKSAS NUMBER: SAMPLED BY: MATERIAL SOURCE:	61303 T. Weiss CENTERLINE, MAIN RUNWAY							

TEST HOLE DEPTH (feel STATION OFFSET LAB NUMBE	t)	TH13-023 1.0-6.0 19+50 CL 13-2173	TH13-023 11.8-12.2 19+50 CL 13-2175	TH13-023 18.3-18.7 19+50 CL 13-2176	TH13-024 3.8-4.2 18+00 20R 13-2177	TH13-024 11.3-11.7 18+00 20R 13-2178	TH13-024 13.8-14.2 18+00 20R 13-2179	TH13-024 18.8-19.2 18+00 20R 13-2180
DATE SAMP	<u>'LED</u>	28-Feb-13	28-Feb-13	28-Feb-13	28-Feb-13	28-Feb-13	28-Feb-13	28-Feb-13
% Passing Gravel	3" 2" 1.5" 1.0" 0.75" 0.5" 0.375" #4	100 99 99						
Sand	#8 #10 #16 #30 #40 #50 #60 #80 #100	98 98 97 97 96 95 95 95 92 90						
Silt/Clay	#200	67.5		!				
Hydro	0.02 0.005 0.002 0.001							
LIQUID LIMIT PLASTIC IND USCS CLAS:	EX SIFICATION	NV NP ML						
USCS SOIL E	DESCRIPTION	SaSi	(SaSi)	(SiSa)	(SiSa)	(SiSa)	(SiSa)	(SiSa)
NATURAL M ORGANICS SP. GR. (FIN SP. GR. (CO) MAX. DRY D OPTIMUM M L.A. ABRASIC DEGRAD. FA SODIUM SUL	DISTURE E) ARSE) ENSITY OISTURE DN ACTOR F. (CRSE)	1.1	25.0	12.5	9.5	8.1 0.5	5.4	8.0
SODIUM SUL NORDIC ABF	.F. (FINE) RASION							
REMARKS								
GENERAL CO	OMMENTS	Gradation is based ¹ Organic content (Soil descriptions USCS Soil Descri	t on material passing determination is bas shown in parenthese ption Abbreviations	g the 3" sieve, accor sed on the results of as are based on field :: WG = Well-grade	ding to Alaska Test the ATM T-6 test m determinations.) 2d; PG = Poorly-gra	Method T-7. 1ethod. 1ded; E = Elastic; I.	, = Lean; F = Fat	

PROJECT NAME:	Ambler Airport Rehibilation
PROJECT NUMBER: AKSAS NUMBER: SAMPLED BY: MATERIAL SOURCE:	61303 T. Weiss CENTERLINE, MAIN RUNWAY

TEST HOLE DEPTH (fee STATION OFFSET LAB NUMBI DATE SAMI	= NUMBER ht) ER PLED	TH13-025 1.3-1.7 15+00 25L 13-2063 16-Feb-13	TH13-025 5.0-10.0 15+00 25L 13-2064 16-Feb-13	TH13-025 11.5-12.0 15+00 25L 13-2066 16-Feb-13	TH13-025 19.5-20.0 15+00 25L 13-2068 16-Feb-13	TH13-026 8.8-9.2 12+50 CL 13-2169 27-Feb-13	TH13-026 13.8-14.2 12+50 CL 13-2170 27-Feb-13	TH13-026 21.5-23.5 12+50 CL 13-2171 27-Feb-13
% Passing Gravel	3" 2" 1.5" 1.0" 0.75" 0.5" 0.375"							
Sand	#4 #8 #10 #16 #30 #40 #50 #60 #80 #100							100 99 98 96 94
Silt/Clay	#200							69.0
Hydro	0.02 0.005 0.002 0.001							
LIQUID LIMI PLASTIC INI USCS CLAS	T DEX SIFICATION							NV NP ML
USCS SOIL :	DESCRIPTION	(SaSi)	(SiSa)	(SiSa)	(SiSa)	(SiSa)	(SiSa)	SaSi
NATURAL M ORGANICS SP. GR. (FIN SP. GR. (CO MAX. DRY D OPTIMUM M L.A. ABRASI DEGRAD. FA SODIUM SU SODIUM SU NORDIC ABI	IOISTURE IE) DARSE) DENSITY IOISTURE ION ACTOR LF. (CRSE) LF. (CRSE) LF. (FINE) RASION	10.2	10.4 0.5	7.5 0.6	27.9	5.4	7.0	
REMARKS								
GENERAL C	OMMENTS	Gradation is based ¹ Organic content (Soil descriptions USCS Soil Descri	determination is bas determination is bas shown in parenthese ption Abbreviations	g the 3" sieve, accord and on the results of es are based on field : WG = Well-grade	ding to Alaska Test the ATM T-6 test m determinations.) 2d; PG ≈ Poorly-gra	Method T-7. nethod. nded; E = Elastic; L	, = Lean; F = Fat	

PROJECT N	IAME:	Ambler Airpo	ort Rehibilation					
PROJECTN	IUMBER:	61303						
SAMPLED E	3Y:	T. Weiss		ESS ROAD RE				
MATERIAL	SOURCE:		L, NEW X001					1400 - 1400 - 1400 - 1400 - 1400 - 1400 - 1400 - 1400 - 1400 - 1400 - 1400 - 1400 - 1400 - 1400 - 1400 - 1400
TEST HOLE DEPTH (fee STATION OFFSET	NUMBER t)	TH13-028 2.3-2.7 1032+00 10B	TH13-028 3.5-8.0 1032+00 10B	TH13-028 5.0-9.5 1032+00 10B	TH13-028 9.5-10.0 1032+00 10R	TH13-027 3.8-4.2 46+00 150R	TH13-027 7.3-7.7 46+00 150R	TH13-027 15.8-16.2 46+00 150R
LAB NUMBE	ĒR	13-2069	13-2070	13-2071	13-2072	13-2153	13-2154	13-2155
DATE SAMP	PLED	18-Feb-13	18-Feb-13	18-Feb-13	18-Feb-13	27-Feb-13	27-Feb-13	27-Feb-13
Gravel	5 2" 1.5" 1.0" 0.75"							
	0.5" 0.375"							
	#4							
	#0 #10							
	#16 #30		100					
Sand	#40		99					
	#50		96 02					
	#60 #80		92 80					
	#100		73					
Silt/Clay	#200		29.3					
Hydro	0.02 0.005 0.002 0.001							
LIQUID LIMI PLASTIC INI USCS CLAS	T DEX SIFICATION		NV NP SM					
USCS SOIL	DESCRIPTION	(SaSi)	SiSa	(SiSa)	(SiSa)	(SiSa)	(SiSa)	(SiSa)
NATURAL M ORGANICS SP. GR. (FIN	OISTURE IE)	11.4	0.4	3.6	5.1 0.5	18.0	6.2	9.9
SP. GR. (CO MAX. DRY D OPTIMUM M L.A. ABRASI DEGRAD. F/ SODIUM SU	ARSE) DENSITY DISTURE ON ACTOR							
SODIUM SU NORDIC AB	LF. (FINE) RASION							
REMARKS								
GENERAL C	OMMENTS	Gradation is base ¹ Organic content (Soil descriptions USCS Soil Descr	d on material passin determination is ba shown in parenthes iption Abbreviation	g the 3" sieve, acco sed on the results of ses are based on fiel s: WG = Well-grad	 rding to Alaska Tes f the ATM T-6 test 1 d determinations.) ed; PG = Poorly-gr	 t Method T-7. nethod. aded; E = Elastic;	L = Lean; F = Fat	I

PROJECT NAME:		Ambler Airpo	ort Rehibilation	i				
PROJECT NUMBER AKSAS NUMBER:	?:	61303						
SAMPLED BY: MATERIAL SOURCI	E:	CENTERLIN	IE, NEW ACCI	ESS ROAD RE	EALIGNMENT			
TEST HOLE NUMBL DEPTH (feet) STATION OFFSET LAB NUMBER DATE SAMPLED	ER	TH13-028 14.5-15.0 1032+00 10R 13-2074 18-Feb-13	TH13-028 19.5-20.0 1032+00 10R 13-2076 18-Feb-13	TH13-029 3.0-8.0 1030+50 20R 13-2186 28-Feb-13	TH13-029 6.8-7.2 1030+50 20R 13-2187 28-Feb-13	TH13-029 14.8-15.2 1030+50 20R 13-2188 28-Feb-13	TH13-029 19.8-20.2 1030+50 20R 13-2189 28-Feb-13	TH13-029 28.8-29.2 1030+50 20R 13-2190 28-Feb-13
% Passing 3" 2"								
1.5" Gravel 1.0" 0.75" 0.5" 0.375" #4								
#8								
#10 #10 #30 #40 #50 #60 #80				100 99 97 94 86				
#100 Silt/Clav #200				81 49.4				
0.02								
Hydro 0.005 0.002 0.001								
LIQUID LIMIT PLASTIC INDEX USCS CLASSIFICAT	TON			NV NP SM				
USCS SOIL DESCRI	PTION	(SiSa)	(SiSa)	SiSa	SiSa	(SiSa)	(SiSa)	(SiSa)
NATURAL MOISTUR ORGANICS SP. GR. (FINE) SP. GR. (COARSE) MAX. DRY DENSITY OPTIMUM MOISTUR L.A. ABRASION DEGRAD. FACTOR SODIUM SULF. (CRS SODIUM SULF. (FINI NORDIC ABRASION	2E 2 2 2 5 5 5 5 5 5 5 5 5 5 7 1 7 1 7 1 7 1 7 1	8.2 0.3	3.2		6.8 0.4	22.6	26.5	22.2
REMARKS								
GENERAL COMMEN	TS	Gradation is based ¹ Organic content (Soil descriptions USCS Soil Descri	l on material passing determination is bas shown in parenthese ption Abbreviations	g the 3" sieve, accor sed on the results of es are based on field s: WG = Well-grade	ding to Alaska Test the ATM T-6 test m l determinations.) xd; PG = Poorly-gra	Method T-7. 1ethod. 1ded; E = Elastic; I	∠ == Lean; F = Fat	

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PROJECT N PROJECT N AKSAS NUN SAMPLED B MATERIAL S	IAME: IUMBER: IBER: SY: SOURCE:	Ambler Airpo 61303 T. Weiss CENTERLIN	ort Rehibilation	ESS ROAD RE	ALIGNMENT			
TEST HOLE DEPTH (feet STATION OFFSET LAB NUMBE DATE SAMF	NUMBER t) ER PLED	TH13-030 3.8-4.2 1026+00 10R 13-2181 28-Feb-13	TH13-030 8.3-8.7 1026+00 10R 13-2182 28-Feb-13	TH13-030 13.3-13.7 1026+00 10R 13-2183 28-Feb-13	TH13-030 18.8-19.2 1026+00 10R 13-2184 28-Feb-13	TH13-031 4.8-5.2 1022+00 5L 13-2263 2-Mar-13	TH13-031 6.8-7.2 1022+00 5L 13-2264 2-Mar-13	TH13-031 9.8-10.2 1022+00 5L 13-2265 2-Mar-13
% Passing Gravel	3" 2" 1.5" 1.0" 0.75" 0.5" 0.375" #4							
Sand	#8 #10 #16 #30 #40 #50 #60 #80 #100							
Silt/Clay	#200							
Hydro	0.02 0.005 0.002 0.001							
LIQUID LIMI PLASTIC INE USCS CLAS	T DEX SIFICATION							
USCS SOIL	DESCRIPTION	(SiSa)	(SiSa)	(SiSa)	(SiSa)	(SiSa)	(SiSa)	(SiSa)
NATURAL M ORGANICS SP. GR. (FIN SP. GR. (CO MAX. DRY D OPTIMUM M L.A. ABRASI DEGRAD. FA SODIUM SU SODIUM SU NORDIC ABI	OISTURE IE) ARSE) DENSITY IOISTURE ON ACTOR LF. (CRSE) LF. (CRSE) LF. (FINE) RASION	12.8	5.1	7.5	8.3	8.9	8.6 0.4	9.4
REMARKS								
GENERAL C	OMMENTS	Gradation is base ' Organic content (Soil descriptions USCS Soil Descr	d on material passin t determination is ba s shown in parenthe ription Abbreviation	ng the 3" sieve, acco used on the results o ses are based on fiel s: WG = Well-grad	rding to Alaska Tes f the ATM T-6 test r d determinations.) led; PG = Poorly-gr	t Method T-7. method. raded; E = Elastic;	L = Lean; F = Fat	

PROJECT N PROJECT N AKSAS NUN SAMPLED E	AME: UMBER: ABER: 3Y:	Ambler Airpo 61303 T. Weiss	ort Rehibilation					
MATERIAL S	SOURCE:	TH13-034	TH13-034	TH13-034	TH13-034	TH13-031	TH13-035	TH13-035
DEPTH (feet STATION OFFSET LAB NUMBE DATE SAMF	t) ER PLED	0.8-1.2 1005+00 CL 13-2249 2-Mar-13	3.0-6.0 1005+00 CL 13-2250 2-Mar-13	10.8-11.2 1005+00 CL 13-2251B 2-Mar-13	13.8-14.2 1005+00 CL 1 3-2252 2-Mar-13	13.3-13.7 1022+00 5L 13-2266 2-Mar-13	1.5-4.5 N67.08265° W157.87454° 13-2281 3-Mar-13	6.0-9.0 N67.08265° W157.87454° 13-2282 3-Mar-13
% Passing Gravel	3" 2" 1.5" 1.0" 0.75" 0.5" 0.375" #4		95 93 93 93 93 93					
Sand	#8 #10 #16 #30 #40 #50 #60 #80 #100		93 93 93 93 93 93 93 92 90 88				100 99 99 97 96	99 98 96 92 89
Silt/Clay	#200		71.6				84.2	53.0
Hydro	0.02 0.005 0.002 0.001							
LIQUID LIMI PLASTIC INL USCS CLAS	T DEX SIFICATION		18 NP ML				20 NP ML	NV NP ML
USCS SOIL	DESCRIPTION	(SiSa)	Si w/Sa	(Si w/Sa)	(Si w/Sa)	(SiSa)	Si w/Sa	SaSi
NATURAL M ORGANICS SP. GR. (FIN SP. GR. (CO MAX. DRY D OPTIMUM M L.A. ABRASI DEGRAD. FA SODIUM SU SODIUM SU NORDIC ABI	OISTURE IE) ARSE) ENSITY OISTURE ON ACTOR LF. (CRSE) LF. (FINE) RASION	21.8 0.5	20.6 0.6	49.0 4.2	58.4	6.7		
REMARKS				sl Org¹				
GENERAL C	OMMENTS	Gradation is base ¹ Organic content (Soil descriptions USCS Soil Descr	d on material passir determination is ba shown in parenthes iption Abbreviation	ng the 3" sieve, acco used on the results o ses are based on fiel s: WG = Well-grad	ording to Alaska Tes f the ATM T-6 test d determinations.) led; PG = Poorly-gr	nt Method T-7. method. raded; E = Elastic;	L = Lean; F = Fat	<u>I</u>

PROJECT N PROJECT N AKSAS NUN	<i>JAME: JUMBER: MBER:</i>	Ambler Airpo	ort Rehibilation					
SAMPLED E MATERIAL :	3Y: SOURCE:	CENTERLIN	IE, LAGOON F	ROAD				
TEST HOLE DEPTH (fee STATION OFFSET LAB NUMBE DATE SAMF	E NUMBER t) ER PLED	TH13-040 4.8-5.2 N67.07924° W157.88278° 13-2272 3-Mar-13	TH13-040 8.8-9.2 N67.07924° W157.88278° 13-2273 3-Mar-13	TH13-040 12.3-12.7 N67.07924° W157.88278° 13-2274 3-Mar-13	TH13-038 5.3-5.7 N67.08102° W157.87937° 13-2276 3-Mar-13	TH13-038 8.3-8.8 N67.08102° W157.87937° 13-2277 3-Mar-13	TH13-036 4.3-4.7 N67.08201° W157.87695° 13-2279 3-Mar-13	TH13-036 10.5-13.0 N67.08201° W157.87695 13-2280 3-Mar-13
% Passing	3"							
Gravel	2" 1.5" 1.0" 0.75" 0.5" 0.375" #4							
Sand	#8 #10 #16 #30 #40 #50 #60 #80 #100							99 99 98 96 94 88 82 69 63
Silt/Clay	#200							39.1
Hydro	0.02 0.005 0.002 0.001							
LIQUID LIMI PLASTIC INI USCS CLAS	T DEX SIFICATION							NV NP SM
USCS SOIL I	DESCRIPTION	(Si w/Sa)	(Si w/Sa)	(SiSa w/Gr)	(SaSi)	(Si w/Sa)	(SaSi)	SiSa
NATURAL M ORGANICS SP. GR. (FIN SP. GR. (CO, MAX. DRY D OPTIMUM M L.A. ABRASI DEGRAD. FA SODIUM SUI SODIUM SUI NORDIC ABP	OISTURE ENSITY OISTURE ON ACTOR LF. (CRSE) LF. (FINE) RASION	27.7 0.5	23.8	15.0	23.6 0.7	16.2	39.5 4.7	24.3
REMARKS							sl Org ¹	
GENERAL C	OMMENTS	Gradation is based ¹ Organic content (Soil descriptions USCS Soil Descri	on material passing determination is bas shown in parenthese ption Abbreviations	g the 3" sieve, accor ed on the results of es are based on field : WG = Well-grade	ding to Alaska Test the ATM T-6 test m determinations.) d; PG = Poorly-gra	Method T-7. ethod. ded; E = Elastic: L	u == Lean; F = Fat	
				5		. /		

PROJECT N PROJECT N AKSAS NUI SAMPLED E MATERIAL	VAME: VUMBER: MBER: BY: SOURCE:	Ambler Airpo 61303 T. Weiss CENTERLIN	ort Rehibilation JE, LAGOON F	ROAD, MAIN A	ND CROSSW	(IND RUNWA)	ſS	
TEST HOLE DEPTH (fee STATION OFFSET LAB NUMBI DATE SAMI	E NUMBER ;t) ER PLED	TH13-044 2.3-2.7 46+50 52L 13-2027 13-Feb-13	TH13-044 0.8-10.2 46+50 52L 13-2029 13-Feb-13	TH13-044 14.3-14.7 46+50 52L 13-2030 13-Feb-13	TH13-045 2.3-2.7 504+00 CL 13-2141 27-Feb-13	TH13-045 8.3-8.7 504+00 CL 13-2143 27-Feb-13	TH13-042 7.3-7.7 N67.07753° W157.88534° 13-2269 3-Mar-13	TH13-042 13.8-14.2 N67.07753° W157.88534 ^t 13-2270 3-Mar-13
% Passing Gravel	3" 2" 1.5" 0.75" 0.5" 0.375" #4							
Sand	#8 #10 #16 #30 #40 #50 #60 #80 #100							
Silt/Clay	#200						T	
Hydro	0.02 0.005 0.002 0.001							
LIQUID LIMI PLASTIC INI USCS CLAS	T DEX SIFICATION							
USCS SOIL	DESCRIPTION	(SaSi)	(SiSa)	(SiSa)	(SiSa)	(Si w/Sa)	(Si w/Sa)	(Si w/Sa)
NATURAL M ORGANICS SP. GR. (FIN SP. GR. (CO MAX. DRY D OPTIMUM M L.A. ABRASI DEGRAD. F/ SODIUM SU SODIUM SU NORDIC AB,	OISTURE IE) VARSE) VENSITY IOISTURE 'ON ACTOR 'LF. (CRSE) 'LF. (FINE) RASION	16.8	9.4	11.6 0.5	12.2 0.7	20.2	22.8 0.5	16.0
REMARKS								
GENERAL C	OMMENTS	Gradation is based ¹ Organic content (Soil descriptions USCS Soil Descri	d on material passing determination is bas shown in parenthes iption Abbreviations	g the 3" sieve, accorsed on the results of es are based on fields: WG = Well-grades	ding to Alaska Test the ATM T-6 test n d determinations.) ed; PG = Poorly-gra	Method T-7. nethod. aded; E = Elastic;	L = Lean; F = Fat	

PROJECT N	IAME:	Ambler Airpo	ort Rehibilation							
PROJECT N AKSAS NUN SAMPLED B MATERIAL S	IUMBER: IBER: IY: SOURCE:	61303 T. Weiss CENTERLINE, MAIN AND CROSSWIND RUNWAYS								
TEST HOLE DEPTH (feet STATION OFFSET LAB NUMBE DATE SAMP	NUMBER ;) ER PLED	TH13-047 1.3-1.7 511+50 20R 13-2082 19-Feb-13	TH13-046 0.8-1.2 42+00 CL 13-2101 23-Feb-13	TH13-046 3.8-4.2 42+00 CL 13-2102 23-Feb-13	TH13-045 14.3-14.7 504+00 CL 13-2144 27-Feb-13	TH13-045 18.8-19.2 504+00 CL 13-2145 27-Feb-13	TH13-045 22.0-25.0 504+00 CL 13-2146 27-Feb-13	TH13-045 28.3-28.7 504+00 CL 13-2147 27-Feb-13		
% Passing Gravel	3" 2" 1.5" 1.0" 0.75" 0.5" 0.375" #4									
Sand	#8 #10 #16 #30 #40 #50 #60 #80 #100						100 99 98 98			
Silt/Clay	#200						82.8			
Hydro	0.02 0.005 0.002 0.001									
LIQUID LIMIT PLASTIC IND USCS CLASS	- DEX SIFICATION						NV NP ML			
USCS SOIL E	DESCRIPTION	(SiSa)	(SaSi)	(Si w/Sa)	(SiSa)	(SiSa)	Si w/Sa	(SaSi)		
NATURAL M ORGANICS SP. GR. (FIN SP. GR. (COA MAX. DRY DE OPTIMUM M L.A. ABRASIC DEGRAD. FA SODIUM SUL SODIUM SUL NORDIC ABR	DISTURE E) ARSE) ENSITY DISTURE DN CTOR .F. (CRSE) .F. (FINE) RASION	21.2	4.9 0.8	19.4	13.4	17.3 0.2		19.3		
REMARKS										
GENERAL CO	DMMENTS	Gradation is based ¹ Organic content (Soil descriptions USCS Soil Descri	t on material passin determination is bas shown in parenthes ption Abbreviations	g the 3" sieve, accor sed on the results of es are based on field :: WG = Well-grade	ding to Alaska Test the ATM T-6 test m l determinations.) ed; PG = Poorly-gra	Method T-7. nethod. Ided; E = Elastic; I				

PROJECT N PROJECT N AKSAS NUN SAMPLED E MATERIAL S	IAME: IUMBER: IBER: 3Y: SOURCE:	Ambler Airpo 61303 T. Weiss CENTERLIN	ort Rehibilation	VIND RUNWAY	YS and OBSTF			
TEST HOLE DEPTH (feel STATION OFFSET LAB NUMBE DATE SAMF	NUMBER t) ER PLED	TH13-047 7.3-7.7 511+50 20R 13-2083 19-Feb-13	TH13-047 10.0-15.0 511+50 20R 13-2085 19-Feb-13	TH13-047 19.5-20.0 511+50 20R 13-2087 19-Feb-13	TH13-049 2.0-10.0 515+00 850L 13-2232 1-Mar-13	TH13-048 2.8-3.2 36+50 600L 13-2234 1-Mar-13	TH13-048 6.8-7.2 36+50 600L 13-2235 1-Mar-13	TH13-048 12.8-13.2 36+50 600L 13-2236 1-Mar-13
% Passing Gravel	3" 2" 1.5" 1.0" 0.75" 0.5" 0.375" #4							
Sand	#8 #10 #16 #30 #40 #50 #60 #80 #100				100 98 96 89 83			
Silt/Clay	#200 0.02				51.4			
Hydro	0.005 0.002 0.001							
LIQUID LIMIT PLASTIC INE USCS CLASS	r DEX SIFICATION				NV NP ML		NV NP	
USCS SOIL [DESCRIPTION	(SiSa)	(SiSa)	(SiSa)	SaSi	(Pt)	(Si w/Sa)	(Si w/Sa)
NATURAL M ORGANICS SP. GR. (FIN SP. GR. (CO) MAX. DRY DI OPTIMUM M L.A. ABRASIC DEGRAD. FA SODIUM SUL SODIUM SUL NORDIC ABF	OISTURE E) ARSE) ENSITY OISTURE ON ACTOR LF. (CRSE) LF. (FINE) RASION	11.1 0.3	6.2 0.2	24.2	0.8	115.5 44.0	31.8	28.4
REMARKS						hi Org ¹		
GENERAL CO	OMMENTS	Gradation is based Organic content (Soil descriptions USCS Soil Descri	d on material passin determination is bas shown in parenthes iption Abbreviations	g the 3" sieve, accor sed on the results of ses are based on field s: WG = Well-grade	rding to Alaska Test 'the ATM T-6 test n d determinations.) ed; PG = Poorly-gra	Method T-7. nethod. aded; E = Elastic;	L = Lean; F = Fat	

PROJECT N	IAME:	Ambler Airpo	ort Rehibilation					
PROJECT N AKSAS NUN SAMPLED B MATERIAL S	IUMBER: MBER: 3Y: SOURCE:	61303 T. Weiss CENTERLIN	IE, MAIN RU'	NWAY and OB	STRUCTION			
TEST HOLE DEPTH (feel STATION OFFSET LAB NUMBE DATE SAMF	NUMBER () ER PLED	TH13-050 0.8-1.2 30+50 25L 13-2109 25-Feb-13	TH13-050 5.0-9.5 30+50 25L 13-2111 25-Feb-13	TH13-050 9.5-10.0 30+50 25L 13-2112 25-Feb-13	TH13-050 14.5-15.0 30+50 25L 13-2114 25-Feb-13	TH13-050 19.5-20.0 30+50 25L 13-2116 25-Feb-13	TH13-051 7.8-8.2 23+00 18L 13-2165 27-Feb-13	TH13-049 14.2-14.8 515+00 850L 13-2233 1-Mar-13
% Passing	3"							
Gravel	2" 1.5" 1.0" 0.75" 0.5" 0.375" #4							
Sand	#8 #10 #16 #30 #40 #50 #60 #80 #100							
Silt/Clay	#200							
Hydro	0.02 0.005 0.002 0.001							
LIQUID LIMI PLASTIC INE USCS CLAS	T DEX SIFICATION							
USCS SOIL I	DESCRIPTION	(SaSi)	(SaSi)	(SaSi)	(SaSi)	(SaSi)	(SaSi)	(SiSa)
NATURAL M ORGANICS SP. GR. (FIN SP. GR. (CO MAX. DRY D OPTIMUM M L.A. ABRASI DEGRAD. FA SODIUM SUI SODIUM SUI NORDIC ABI	OISTURE ARSE) ENSITY OISTURE ON ACTOR LF. (CRSE) LF. (FINE) RASION	7.1	18.6	18.2	22.5 0.5	28.2	17.8	9.4
REMARKS								
GENERAL C	OMMENTS	Gradation is base ¹ Organic content (Soil descriptions USCS Soil Descr	d on material passir determination is ba shown in parenthes iption Abbreviation	l ng the 3" sieve, acco used on the results of ses are based on field is: WG = Well-grad	rding to Alaska Test f the ATM T-6 test r d determinations.) ed; PG = Poorly-gr	It Method T-7. nethod. aded; E = Elastic;	L = Lean; F = Fat	

PROJECT N PROJECT N AKSAS NUN SAMPLED E MATERIAL :	IAME: IUMBER: MBER: 3Y: SOURCE:	Ambler Airpo 61303 T. Weiss CENTERLIN	ort Rehibilation IE, MAIN RU	NWAY, PARKI	ING APRON A	ND TAXIWAY		
TEST HOLE DEPTH (feet STATION OFFSET LAB NUMBE DATE SAMF	ENUMBER t) ER PLED	TH13-053 3.2-3.7 103+50 100R 13-2004 12-Feb-13	TH13-053 4.0-7.0 103+50 100R 13-2005 12-Feb-13	TH13-053 7.8-8.2 103+50 100R 13-2006 12-Feb-13	TH13-052 6.8-7.2 101+00 30L 13-2019 12-Feb-13	TH13-052 10.2-10.7 101+00 30L 13-2020 12-Feb-13	TH13-051 13.3-13.7 23+00 18L 13-2166 27-Feb-13	TH13-051 16.8-17.2 23+00 18L 13-2167 27-Feb-13
% Passing Gravel	3" 2" 1.5" 1.0" 0.75" 0.5" 0.375" #4							
Sand	#8 #10 #16 #30 #40 #50 #60 #80 #100		100 99 99 96 95					
Silt/Clay	#200 0.02		75.7					
Hydro	0.005 0.002 0.001							
LIQUID LIMIT PLASTIC INE USCS CLAS	T DEX SIFICATION	NV NP	NV NP ML				NV NP	
USCS SOIL [DESCRIPTION	(Si w/Sa)	Si w/Sa	(SaSi)	(SiSa)	(SiSa)	(SaSi)	(SaSi)
NATURAL M ORGANICS SP. GR. (FIN SP. GR. (CO, MAX. DRY D OPTIMUM M L.A. ABRASI DEGRAD. FA SODIUM SUI SODIUM SUI NORDIC ABF	OISTURE E) ARSE) ENSITY OISTURE ON ACTOR LF. (CRSE) LF. (CRSE) RASION	24.9 0.6		24.7	10.0 0.5	9.1	20.0	22.9
REMARKS								
GENERAL CO	OMMENTS	Gradation is based ¹ Organic content (Soil descriptions USCS Soil Descri	t on material passing determination is bas shown in parenthes ption Abbreviations	g the 3" sieve, accor sed on the results of es are based on field s: WG = Well-grade	ding to Alaska Test the ATM T-6 test n I determinations.) ed; PG = Poorly-gra	Method T-7. nethod. aded; E = Elastic; 1	L = Lean; F = Fat	

PROJECT	IAME:	Ambler Airpo	ort Rehibilation					
PROJECT N AKSAS NUN SAMPLED E MATERIAL S	IUMBER: MBER: 3Y: SOURCE:	61303 T, Weiss CENTERLIN	IE, PARKING	APRON AND	ACCESS RO	٩D		
TEST HOLE DEPTH (fee STATION OFFSET LAB NUMBE DATE SAMF	NUMBER t) ER PLED	TH13-054 8.2-8.7 103+00 300R 13-2001 12-Feb-13	TH13-054 9.0-13.0 103+00 300R 13-2002 12-Feb-13	TH13-054 14.3-14.7 103+00 300R 13-2003 12-Feb-13	TH13-053 13.8-14.2 103+50 100R 13-2007 12-Feb-13	TH13-053 17.8-18.2 103+50 100R 13-2008 12-Feb-13	TH13-055 4.8-5.2 1001+00 5L 13-2246 2-Mar-13	TH13-055 8.3-8.7 1001+00 5L 13-2247 2-Mar-13
% Passing	3" 2"							
Gravel	- 1.5" 1.0" 0.75" 0.5" 0.375" #4							
Sand	#8 #10 #16 #30 #40 #50 #60 #80 #100		100 99 98 97					
Silt/Clay	#200		77.8					
Hydro	0.002 0.005 0.002 0.001							
LIQUID LIMI PLASTIC INE USCS CLAS	r DEX SIFICATION		NV NP ML					
USCS SOIL L	DESCRIPTION	(Si w/Sa)	Si w/Sa	(Si w/Sa)	(SiSa)	(SaSi)	(Si w/Sa)	(Si w/Sa)
NATURAL M ORGANICS SP. GR. (FIN SP. GR. (CO, MAX. DRY D, OPTIMUM M L.A. ABRASIG DEGRAD. FA SODIUM SUL SODIUM SUL NORDIC ABF	OISTURE E) ARSE) ENSITY OISTURE ON ICTOR .F. (CRSE) .F. (FINE) RASION	26.1		20.4	12.8	14.2	21.7 0.6	22.8
REMARKS								
GENERAL C	OMMENTS	Gradation is based ' Organic content (Soil descriptions USCS Soil Descri	on material passing determination is bas shown in parenthese ption Abbreviations	y the 3" sieve, accor- ed on the results of es are based on field : WG = Well-grade	ding to Alaska Test the ATM T-6 test m determinations.) ed; PG = Poorly-gra	Method T-7. nethod. ded; E = Elastic; L	∠ = Lean; F = Fat	

PROJECT NAME PROJECT NUME AKSAS NUMBEF SAMPLED BY: MATERIAL SOUL	:: 3ER: R: RCE:	Ambler Airpo 61303 T. Weiss CENTERLIN	ort Rehibilation	ROAD AND N	OT CONSIDEF	RED PARKING	APRON	
TEST HOLE NUM DEPTH (feet) STATION OFFSET LAB NUMBER DATE SAMPLED	ABER	TH13-059 3.5-7.0 102+50 200L 13-2010 12-Feb-13	TH13-059 8.8-9.2 102+50 200L 13-2011 12-Feb-13	TH13-055 12.3-12.7 1001+00 5L 13-2248 2-Mar-13	TH13-056 0.0-3.0 1009+00 5L 13-2255 2-Mar-13	TH13-057 3.0-8.0 1017+50 5L 1 3-2259 2-Mar-13	TH13-057 3.3-3.7 1017+50 5L 13-2260 2-Mar-13	TH13-057 13.8-14.2 1017+50 5L 13-2261 2-Mar-13
% Passing 3" 2" 1.5 Gravel 1.0 0.7 0.5 0.3 #4	" 5" "75"				99 97 91			
#8 #10 #30 Sand #40 #50 #60 #80 #10) ;)))))))	100 98 97 94 91			86 84 77 67 62 56 53 46 42	100 99 99 98 96 95		
Silt/Clay #20 0.0	10	51.3			28.3	72.1		
Hydro 0.00 0.00 0.00	05 02 01							
LIQUID LIMIT PLASTIC INDEX USCS CLASSIFIC	CATION	NV NP ML				NV NP ML		
USCS SOIL DESC	RIPTION	SaSi	(SiSa)	(Si w/Sa)	SiSa	Si w/Sa	Si w/Sa	(SiSa)
NATURAL MOIST ORGANICS SP. GR. (FINE) SP. GR. (COARSE MAX. DRY DENSI OPTIMUM MOIST L.A. ABRASION DEGRAD. FACTO SODIUM SULF. (C SODIUM SULF. (F NORDIC ABRASIC	URE E) ITY URE IR CRSE) EINE) ON	0.6	7.1	32.7 3.9	1.0	2.2	6.9	9.2
REMARKS				sl Org¹		sl Org ¹		
GENERAL COMM	ENTS	Gradation is based ¹ Organic content of (Soil descriptions of USCS Soil Descriptions	l on material passing determination is bas shown in parenthese ption Abbreviations	2 the 3" sieve, accor sed on the results of es are based on field :: WG = Well-grade	ding to Alaska Test the ATM T-6 test m l determinations.) 2d; PG = Poorly-gra	Method T-7. nethod. nded; E = Elastic; I	∠ = Lean; F = Fat	

PROJECT NAI PROJECT NUI AKSAS NUMB SAMPLED BY: MATERIAL SO	ME: MBER: ER: WRCE:	Ambler Airpo 61303 T. Weiss CENTERLIN	ort Rehibilation	SIDERED PAR	RKING APRON	I AND SREB A	AREA	
TEST HOLE N DEPTH (feet) STATION OFFSET LAB NUMBER DATE SAMPLE	UMBER ED	TH13-059 13.8-14.2 102+50 200L 13-2012 12-Feb-13	TH13-059 21.8-22.2 102+50 200L 13-2013 12-Feb-13	TH13-060 2.8-3.2 102+50 50L 13-2014 12-Feb-13	TH13-060 7.3-7.8 102+50 50L 13-2015 12-Feb-13	TH13-060 10.3-10.7 102+50 50L 13-2016 12-Feb-13	TH13-060 14.3-14.7 102+50 50L 13-2017 12-Feb-13	TH13-061 1.8-2.2 102+50 200L 13-2056 16-Feb-13
% Passing 3 2 1 Gravel 1 0 0 0 4	3" 2" 1.0").75").5").375" 44							
# # # Sand # # # #	48 410 430 440 450 460 480 480							
Silt/Clay #	\$200							
Hydro 0 0 0).02).005).002).001							
LIQUID LIMIT PLASTIC INDE; USCS CLASSIF	X FICATION							
USCS SOIL DE	SCRIPTION	(SiSa)	(SiSa)	(SiSa)	(SiSa)	(SiSa)	(SiSa)	(SiSa)
NATURAL MOIS ORGANICS SP. GR. (FINE) SP. GR. (COAR MAX. DRY DEN OPTIMUM MOIS L.A. ABRASION DEGRAD. FAC SODIUM SULF. SODIUM SULF. NORDIC ABRAS	STURE ISITY STURE I TOR (CRSE) (FINE) SION	9.5	10.1	6.6	8.6	8.6	9.5	18.3 0.7
REMARKS								
GENERAL CON	IMENTS	Gradation is based ¹ Organic content of (Soil descriptions) USCS Soil Descriptions	on material passing determination is bas shown in parenthes ption Abbreviations	g the 3" sieve, accor sed on the results of es are based on field :: WG = Well-grade	ding to Alaska Test the ATM T-6 test m determinations.) rd; PG = Poorly-gra	Method T-7. ethod. ded; E = Elastic; I	. = Lean; F = Fat	L

4

Ambler Airport Rehibilation

PROJECT NAME: PROJECT NUMBER: AKSAS NUMBER: SAMPLED BY: MATERIAL SOURCE:

61303 T. Weiss CENTERLINE, NOT CONSIDERED SREB AREA

TEST HOLE DEPTH (fee STATION OFFSET LAB NUMBE DATE SAMF	E NUMBER t) ER PLED	TH13-061 4.5-8.0 102+50 200L 13-2057 16-Feb-13	TH13-061 10.0-12.0 102+50 200L 13-2058 16-Feb-13	TH13-061 16.5-17.0 102+50 200L 13-2060 16-Feb-13	TH13-061 24.5-25.0 102+50 200L 13-2062 16-Feb-13	TH13-062 5.0-10.0 N67.10127° W157.85584° 13-2130 26-Feb-13	TH13-062 28.8-29.2 N67.10127° W157.85584° 13-2134 26-Feb-13	TH13-062 25.0-30.0 N67.10127° W157.85584° 13-2135 26-Feb-13
% Passing Gravel	3" 2" 1.5" 1.0" 0.75" 0.5" 0.375" #4							
Sand	#8 #10 #16 #30 #40 #50 #60 #80 #100	100 99 98 97 92 92						100 98 95 87 82
Silt/Clay	#200	67.6						64.5
Hydro	0.02 0.005 0.002 0.001							
LIQUID LIMI PLASTIC INI USCS CLAS	T DEX SIFICATION	N∨ NP ML						NV NP ML
USCS SOIL	DESCRIPTION	SaSi	(SiSa)	(SiSa)	(SiSa)	(SiSa)	(SaSi)	SaSi
NATURAL M ORGANICS SP. GR. (FIN SP. GR. (CO MAX. DRY D OPTIMUM M L.A. ABRASI DEGRAD. F/ SODIUM SU SODIUM SU NORDIC AB	IOISTURE IE) DENSITY IOISTURE ION ACTOR LF. (CRSE) LF. (FINE) RASION	1.2	15.7	6.8	22.7	7.6	18.6	28.8
REMARKS								
GENERAL C	COMMENTS	Gradation is base ' Organic content (Soil descriptions USCS Soil Descr	d on material passir determination is ba s shown in parenthes iption Abbreviation	ng the 3" sieve, acco sed on the results o ses are based on fiel s: WG = Well-grad	rding to Alaska Tes f the ATM T-6 test d determinations.) ed; PG = Poorly-gr	t Method T-7. nethod. aded; E = Elastic;	L = Lean; F = Fat	

Ambler Airport Rehibilation

PROJECT NAME: PROJECT NUMBER: AKSAS NUMBER: SAMPLED BY: MATERIAL SOURCE:

61303 T. Weiss CENTERLINE, NOT CONSIDERED SREB AREA

TEST HOLE DEPTH (fee STATION OFFSET LAB NUMBE DATE SAMF	E NUMBER t) ER PLED	TH13-063 1.0-4.5 N67.10147° W157.85573° 13-2040 14-Feb-13	TH13-063 4.5-5.0 N67.10147° W157.85573° 13-2041 14-Feb-13	TH13-063 5.0-9.0 N67.10147° W157.85573° 13-2042 14-Feb-13	TH13-063 9.0-9.5 N67.10147° W157.85573° 13-2043 14-Feb-13	TH13-063 9.5-11.5 N67.10147° W157.85573° 13-2044 14-Feb-13	TH13-063 22.3-22.7 N67.10147° W157.85573° 13-2045 14-Feb-13	TH13-063 27.8-28.2 N67.10147° W157.85573° 13-2046 14-Feb-13
% Passing Gravel	3" 2" 1.5" 1.0" 0.75" 0.5" 0.375" #4							
Sand	#8 #10 #16 #30 #40 #50 #60 #80 #100	99 99 98 96 95 93 92 88 88 86		100 99 97 95 88 83				
Silt/Clay	#200	67.5		48.0				
Hydro	0.02 0.005 0.002 0.001							
LIQUID LIMI PLASTIC INI USCS CLAS	T DEX SIFICATION							
USCS SOIL	DESCRIPTION	SaSi	(SiSa)	SiSa	(SiSa)	(SiSa)	(SaSi)	(SaSi)
NATURAL M ORGANICS SP. GR. (FIN SP. GR. (CO MAX. DRY D OPTIMUM M L.A. ABRASI DEGRAD. FA SODIUM SU SODIUM SU NORDIC ABI	IOISTURE IE) DARSE) DENSITY IOISTURE ION ACTOR ILF. (CRSE) LF. (FINE) RASION	2.2	6.9		5.5 0.4	7.0	25.2	25.5
REMARKS		sl Org ¹						
GENERAL C	COMMENTS	Gradation is base ¹ Organic content (Soil descriptions USCS Soil Descr	d on material passir determination is ba s shown in parenthes iption Abbreviation	ng the 3" sieve, acco sed on the results of ses are based on fiel s: WG = Well-grad	, the ATM T-6 test to d determinations.) ed; PG == Poorly-gr	t Method T-7. nethod. aded; E = Elastic;	L = Lean; F = Fat	

PROJECT N	IAME:	Ambler Airport Rehibilation							
PROJECT N AKSAS NUM SAMPLED B MATERIAL S	IUMBER: IBER: BY: SOURCE:	61303 T. Weiss CENTERLIN	IE, NOT CON	SIDERED SRE	EB AREA				
TEST HOLE	NUMBER	TH13-065	TH13-065	TH13-065	TH13-065	TH13-064	TH13-064	TH13-064	
DEPTH (feet	t)	1.0-3.0	4.0-6.0	13.8-14.2	15.0-17.0	2.3-2.7	6.8-7.2	5.0-10.0	
STATION		N67.10166°	N67.10166°	N67.10166°	N67.10166°	N67.10168°	N67.10168°	N67.10168°	
OFFSET		W157.85554°	W157.85554°	W157.85554°	W157.85554°	W157.85594°	W157.85594°	W157.85594°	
LAB NUMBE	ĒR	13-2048	13-2049	13-2052	13-2053	13-2136	13-2137	13-2138	
DATE SAMF	PLED	15-Feb-13	15-Feb-13	15-Feb-13	15-Feb-13	26-Feb-13	26-Feb-13	26-Feb-13	
% Passing	3"								
-	2"								
	1.5"								
Querial	1.0"								
Gravei	0.75"								

Gravel	1.0" 0.75" 0.5" 0.375" #4							
Sand	#8 #10 #16 #30 #40 #50 #60 #80 #100	100 99 98 97 96 95 94						100
Silt/Clay	#200	81.4						91.2
Hydro	0.02 0.005 0.002 0.001							
LIQUID LIMIT PLASTIC IND USCS CLASS	F DEX SIFICATION	20 NP ML						NV NP ML
USCS SOIL I	DESCRIPTION	Si w/Sa	(SiSa)	(SiSa)	(SiSa)	(SiSa)	Si	Si
NATURAL M ORGANICS SP. GR. (FIN SP. GR. (CO, MAX. DRY D OPTIMUM M L.A. ABRASIC DEGRAD. FA SODIUM SUL SODIUM SUL NORDIC ABF	OISTURE E) ARSE) ENSITY OISTURE ON ICTOR .F. (CRSE) .F. (FINE) RASION	0.5	3.6	10.0	0.7	8.8	10.9	12.3
REMARKS								
GENERAL C	OMMENTS	Gradation is base ¹ Organic content (Soil descriptions USCS Soil Descr	d on material passir determination is ba shown in parenthe: iption Abbreviation	I mg the 3" sieve, acco used on the results of ses are based on fiel s: WG = Well-grad	t rding to Alaska Tes f the ATM T-6 test o d determinations.) ed; PG = Poorly-gr	L t Method T-7. nethod. aded; E = Elastic; 1	I L = Lean; F == Fat	1

PROJECT N	IAME:	Ambler Airpo	ort Rehibilation	I				
PROJECT N	IUMBER:	61303						
SAMPLED B	BY:	T. Weiss			ER AREA			
MATERIALS	SOURCE:							
TEST HOLE	NUMBER	TH13-065	TH13-065					
DEPTH (feet	t)	17.5-20.0 N67 10166°	20.0-22.0 N67 10166°					
OFFSET		W157.85554°	W157.85554°					
LAB NUMBE	R N FD	13-2054	13-2055					
% Passing	3"	10-10-10						
-	2"							
	1.5" 1.0"							
Gravei	0.75"							
	0.5" 0.375"							
	#4							
	#8 #10			Į				
	#16							
Sand	#30 #40	100						
	#50	98						
	#60 #80	97 01						
	#80 # <u>100</u>	88						
Silt/Clay	#200	59.2						
L lu selvo	0.02 0.005							
Hyaro	0.002							
	0.001	06						
PLASTIC INE	DEX	26 NP						1
USCS CLASS	SIFICATION	ML						1
USCS SOIL L	DESCRIPTION	SaSi	(SiSa)					1
NATURALA	~!~TUDE							, I
ORGANICS	UISTUKE		13.0					
SP. GR. (FIN	E)							
SP. GR. (CO) MAX. DRY D	ARSE) ENSITY							
OPTIMUM M	OISTURE							
L.A. ABRASIO	ON CTOR							
SODIUM SUL	.F. (CRSE)							
SODIUM SUL	.F. (FINE)							
	NASION .							
REMARKS								
GENERAL CO	OMMENTS	Gradation is based	l on material passin determination is ba	g the 3" sieve, acco sed on the results of	rding to Alaska Test the ATM T-6 test v	Method T-7.		
		(Soil descriptions	shown in parenthes	es are based on field	determinations.)			
		USCS Soil Descri	ption Abbreviation:	s: WG = Well-grad	ed; PG = Poorly-gra	aded; E = Elastic; I	. = Lean; F = Fat	

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APPENDIX C: NATURALLY OCCURRING ASBESTOS LABORTORY TEST RESULTS:



Page 94



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Client:			EMSL Refere
	Alaska Dept. of Transport	ation	
	2301 Peger Rd.		
	Fairbanks, AK 99709		Date Recei
Attention:	Timothy Weiss		Date Analy:
Fax:	(907) 451-2353 Pho	ne: (907) 458-6883	Date Repor
Project:	AMBLEC AIRPORT / # 6	1303	

EMSL Reference: 091303718

 Date Received:
 03/12/13

 Date Analyzed:
 03/18/13

 Date Reported:
 03/19/13

Asbestos Analysis of Bulk Samples via Modified EPA 600/R-93/116 Method Utilizing Analytical Electron Microscopy (Section 2.5.5.2) with CARB 435 Prep (Milling) Level B for 0.1% Target Analytical Sensitivity

Client Sample ID	EMSL Sample ID	Asbestos Type(s)	# of Asbestos Structures Detected	Analytical Sensitivity %	Asbestos Weight %	Comments
13-2089	091303718-0001	Chrysotile	1	0.1	<0.1	
13-2037	091303718-0002	None Detected	None Detected	0.1	<0.1	
13-2214	091303718-0003	None Detected	None Detected	0.1	<0.1	
13-2216	091303718-0004	None Detected	None Detected	0.1	<0.1	
13-2220	091303718-0005	None Detected	None Detected	0.1	<0.1	
13-2224	091303718-0006	None Detected	None Detected	0.1	<0.1	
13-2226	091303718-0007	Chrysotile	1	0.1	<0.1	
13-2237	091303718-0008	None Detected	None Detected	0.1	<0.1	245,
13-2239	091303718-0009	None Detected	None Detected	0.1	<0.1	
13-2244	091303718-0010	None Detected	None Detected	0.1	<0.1	
13-2118	091303718-0011	None Detected	None Detected	0.1	<0.1	
13-2174	091303718-0012	None Detected	None Detected	0.1	<0.1	
13-2262	091303718-0013	None Detected	None Detected	0.1	<0.1	
13-2271	091303718-0014	None Detected	None Detected	0.1	<0.1	
13-2278	091303718-0015	None Detected	None Detected	0.1	<0.1	



Client:			EMSL Reference:	091303718
	Alaska Dept. of Tra	nsportation		
	2301 Peger Rd.			
	Fairbanks, AK 9970	9	Date Received:	03/12/13
Attention:	Timothy Weiss		Date Analyzed:	03/18/13
Fax:	(907) 451-2353	Phone: (907) 458-6883	Date Reported:	03/19/13
Project:	AMBLEC AIRPORT	/ # 61303		

Asbestos Analysis of Bulk Samples via Modified EPA 600/R-93/116 Method Utilizing Analytical Electron Microscopy (Section 2.5.5.2) with CARB 435 Prep (Milling) Level B for 0.1% Target Analytical Sensitivity

Client Sample ID	EMSL Sample ID	Asbestos Type(s)	# of Asbestos Structures Detected	Analytical Sensitivity %	Asbestos Weight %	Comments
13-2230	091303718-0016	Chrysotile	2	0.1	0.1	
13-2110	091303718-0017	None Detected	None Detected	0.1	<0.1	
13-2245	091303718-0018	Chrysotile	2	0.1	<0.1	
13-2253	091303718-0019	None Detected	None Detected	0.1	<0.1	

Analysts

Ken Dunbar (19)

Approved EMSL Signatory

EMSL maintains liability limited to cost of analysis. This method requires the laboratory to analyze the sample until the first fiber found compromises 5% of the total mass. Due to the size and mass of different asbestos fibers, the analytical sensitivity will vary between samples and may prevent the laboratory from achieving the target sensitivity on all samples. This report relates only to the samples reported above and may not be reproduced, except in full, without written approval by EMSL. EMSL is not responsible for sample collection activities or analytical method limitations. Interpretation and use of results are the responsibility of the client.



Client:			EMSL Reference:
	Alaska Dept. of Tr	ansportation	
	2301 Peger Rd.		
	Fairbanks, AK 997	'09	Date Received:
Attention:	Timothy Weiss		Date Analyzed:
Fax:	(907) 451-2353	Phone: (907) 458-6883	Date Reported:
Project:	AMBLER AIRPOR	T / # 61303	

091304456

03/23/13 03/29/13 03/30/13

Asbestos Analysis of Bulk Samples via Modified EPA 600/R-93/116 Method Utilizing Analytical Electron Microscopy (Section 2.5.5.2) with CARB 435 Prep (Milling) Level B for 0.1% Target Analytical Sensitivity

Client Sample ID	EMSL Sample ID	Asbestos Type(s)	# of Asbestos Structures Detected	Analytical Sensitivity %	Asbestos Weight %	Comments
13-2195	091304456-0001	Chrysotile	14	0.1	<0.1	
13-2197	091304456-0002	Chrysotile	1	0.1	<0.1	alendal konstan un proprio de la constante de la constante anti-
13-2021	091445618-0003	Chrysotile	3	0.1	<0.1	
13-2090	091304456-0004	Chrysotile	8	0.1	<0.1	
13-2031	091304456-0005	Chrysotile	74	0.1	0.2	
13-2032	091304456-0006	Chrysotile	3	0.1	<0.1	
13-2148	091304456-0007	Chrysotile	5	0.1	<0.1	
13-2219	091304456-0008	Chrysotile	1	0.1	<0.1	
13-2225	091304456-0009	Chrysotile	1	0.1	<0.1	
13-2200	091304456-0010	None Detected	None Detected	0.1	<0.1	
13-2202	091304456-0011	Chrysotile	1	0.1	<0.1	
13-2208	091304456-0012	None Detected	None Detected	0.1	<0.1	
13-2207	091304456-0013	Chrysotile	1	0.1	<0.1	
13-2211	091304456-0014	Chrysotile	3	0.1	<0.1	
13-2243	091304456-0015	None Detected	None Detected	0.1	<0.1	



Client:			EMSL Reference:	091304456
	Alaska Dept. of Tra	insportation		
	2301 Peger Rd.			
	Fairbanks, AK 9970)9	Date Received:	03/23/13
Attention:	Timothy Weiss		Date Analyzed:	03/29/13
Fax:	(907) 451-2353	Phone: (907) 458-6883	Date Reported:	03/30/13
Project:	AMBLER AIRPORT	Г / # 61303		

Asbestos Analysis of Bulk Samples via Modified EPA 600/R-93/116 Method Utilizing Analytical Electron Microscopy (Section 2.5.5.2) with CARB 435 Prep (Milling) Level B for 0.1% Target Analytical Sensitivity

Client Sample ID	EMSL Sample ID	Asbestos Type(s)	# of Asbestos Structures Detected	Analytical Sensitivity %	Asbestos Weight %	Comments
13-2104	091304456-0016	Chrysotile	23	0.1	0.1	
13-2244	091304456-0017	Chrysotile	12	0.1	<0.1	
13-2077	091304456-0018	Chrysotile	36	0.1	<0.1	
13-2157	091304456-0019	Chrysotile	43	0.1	<0.1	
13-2160	091304456-0020	Chrysotile	50	0.1	<0.1	
13-2161	091304456-0021	Chrysotile	22	0.1	<0.1	

Analysts

Rui Cindy Geng (12) Ken Dunbar (9)

Approved EMSL Signatory

EMSL maintains liability limited to cost of analysis. This method requires the laboratory to analyze the sample until the first fiber found compromises 5% of the total mass. Due to the size and mass of different asbestos fibers, the analytical sensitivity will vary between samples and may prevent the laboratory from achieving the target sensitivity on all samples. This report relates only to the samples reported above and may not be reproduced, except in full, without written approval by EMSL. EMSL is not responsible for sample collection activities or analytical method limitations. Interpretation and use of results are the responsibility of the client.

Client:	Alaska Dept. of Transportation 2301 Peger Rd. Fairbanks, AK 99709	EMSL Reference:	091304916	EMBL ANALYTICAL, INC
		Date Received:	04/02/13	
Attention:	Timothy Weiss	Date Analyzed:	04/08/13	
Fax: Project:	(907) 451-2353 Phone: (907) 458-6883 AMBLER AIRPORT / # 61303	Date Reported:	04/09/13	

EMS

Asbestos Analysis of Bulk Samples via Modified EPA 600/R-93/116 Method Utilizing Analytical Electron Microscopy (Section 2.5.5.2) with CARB 435 Prep (Milling) Level B for 0.1% Target Analytical Sensitivity

Client Sample ID	EMSL Sample ID	Asbestos Type(s)	# of Asbestos Structures Detected	Analytical Sensitivity %	Asbestos Weight %	Comments
13-2036B	091304916-0001	CHRYSOTILE	3	0.1	<0.1	
13-2172	091304916-0002	NONE DETECTED	0	0.1	<0.1	ngaranaranan aran dan karanan dan karan
13-2168	091304916-0003	NONE DETECTED	0	0.1	<0.1	
13-2185	091304916-0004	CHRYSOTILE	1	0.1	<0.1	
13-2186	091304916-0005	NONE DETECTED	0	0.1	<0.1	
13-2256	091304916-0006	CHRYSOTILE	56	0.1	0.2	
13-2257	091304916-0007	CHRYSOTILE	51	0.1	0.1	
13-2250	091304916-0008	CHRYSOTILE	1	0.1	<0.1	
13-2281	091304916-0009	CHRYSOTILE	2	0.1	<0.1	
13-2275	091304916-0010	CHRYSOTILE	9	0.1	0.1	-
13-2268	091304916-0011	CHRYSOTILE	2	0.1	<0.1	
13-2028	091304916-0012	NONE DETECTED	0	0.1	<0.1	
13-2142	091304916-0013	NONE DETECTED	0	0.1	<0.1	
13-2164	091304916-0014	NONE DETECTED	0	0.1	<0.1	
13-2005	091304916-0015	CHRYSOTILE	1	0.1	<0.1	
13-2000	091304916-0016	CHRYSOTILE	1	0.1	<0.1	
13-2254	091304916-0017	CHRYSOTILE	51	0.1	0.1	

Page 1 of 2



Client:	Alaska Dept. of Transportation 2301 Peger Rd. Fairbanks, AK 99709	EM
Attention:	Timothy Weiss	D
Fax:	(907) 451-2353 Phone: (907) 458-6883	D
Project:	AMBLER AIRPORT / # 61303	D

EMSL Reference: 091304916

ate Received: 04/02/13 ate Analyzed: 04/08/13 ate Reported: 04/09/13

Asbestos Analysis of Bulk Samples via Modified EPA 600/R-93/116 Method Utilizing Analytical Electron Microscopy (Section 2.5.5.2) with CARB 435 Prep (Milling) Level B for 0.1% Target Analytical Sensitivity

Client	EMSL	Asbestos	# of Asbestos	Analytical	Asbestos	
Sample ID	Sample ID	Type(s)	Structures	Sensitivity	Weight	Comments
·	,	91 ()	Detected	%	%	
		NONE				
13-2258	091304916-0018	NONE	0	0.1	<0.1	
**************************************		DETECTED	-			
10 0050	001204040 0010		0	0.4	10.4	
13-2259	091304916-0019	CHRYSOTILE	6	0.1	<0.1	
Differentiation (1974) (1974) (1974) (1974) (1974) (1974) (1974) (1974) (1974) (1974) (1974) (1974) (1974) (1974)		NONE				
13-2009	091304916-0020	NONE	0	0.1	<0.1	
радилиционных вородор. «««	1944	DETECTED	an a succession of the state of			
13-2047	091304916-0021	NONE	0	0.1	<0.1	
10 20 11		DETECTED	U	0.1	-0.1	
13 2245	001304016 0022		41	0.1	0.2	
10-2240	091304910-0022	OHNISOTILL	41	0.1	0.2	
13-2018	091304916-0023	CHRYSOTILE	1	0.1	<0.1	
Constanting of the second s						
12 2221	001204016 0024	NONE	0	0.1	-0.1	
15-2231	091304910-0024	DETECTED	0	0.1	~ 0.1	
Million and a state of the second state of the						

Analysts

Ken Dunbar (24)

Approved EMSL Signatory

EMSL maintains liability limited to cost of analysis. This method requires the laboratory to analyze the sample until the first fiber found compromises 5% of the total mass. Due to the size and mass of different asbestos fibers, the analytical sensitivity will vary between samples and may prevent the laboratory from achieving the target sensitivity on all samples. This report relates only to the samples reported above and may not be reproduced, except in full, without written approval by EMSL. EMSL is not responsible for sample collection activities or analytical method limitations. Interpretation and use of results are the responsibility of the client.

APPENDIX D: THERMISTOR RESULTS

Ambler Airport Rehabilitation-Main Runway at TH13-019

Sensor Number	Depth (feet)	27-Feb.	28-Feb.	1-Mar.	2-Mar.	4-Mar.
1	1.5	7.8	8.0	8.5	8.6	8.7
2	2.5	11.6	11.8	11.8	12.0	12.0
3	4.5	18.7	18.6	18.4	18.3	18.1
4	6.5	24.8	24.6	24.4	24.1	23.8
5	8.5	28.7	28.6	28.5	28.3	28.0
6	13.5	32.1	32.1	32.1	32.1	32.1
7	18.5	32.1	32.2	32.2	32.1	32.2

Ground Temperatures (Fahrenheit)

Notes:

1. TH13-019 drilled February 19, 2013 and cable installed on the same date.

2. Datalogger set to take hourly readings; selected readings are presented here.

Ambler Airport Rehabilitation-Not Considered Proposed SBEB Area at TH13-065

Sensor Number	Depth (feet)	16-Feb.	19-Feb.	22-Feb.	24-Feb.	26-Feb.
1	0.5	17.3	4.0	0.8	0.6	4.2
2	2.5	24.6	18.5	12.9	12.1	11.1
3	4.5	28.7	27.3	24.8	24.2	22.9
4	9.5	32.0	33.0	33.0	33.0	32.9
5	14.5	34.7	34.6	34.4	34.4	34.4
6	19.5	35.6	35.5	35.5	35.4	35.4
7	24.5	35.6	35.5	35.5	35.5	35.5
8	29.5	35.6	35.6	35.6	35.6	35.6

Ground Temperatures (Fahrenheit)

Notes:

1. TH13-065 drilled February 15, 2013 and cable installed the same date.

3. Datalogger set to take twice daily readings; selected readings are presented here.

APPENDIX E: PREVIOUS TEST HOLE LOCATIONS AND RESULTS







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				14		
						5
				Proj. ·	-	
				AMBLE	R AIF	RPORT
				10.		
					1	
84				Vert -	1 1	OFIZ.
X4 45				Vert 3	H O	oriz.
14 23				Vert 3	O	tert CC
रत भुग	1. 10 - 11 1			Vert 2	O O	teriz. Teri CC
ति <u>२</u>		-		Vert 3		oriz. Net CC
4 31 54 31			• • • •	Vert 1	0	oriz. Teer CC
14 31 84 31			-	Vert 3	H 0	oriz. Net CC
14 31 84 31				Vert j	0	oriz. Net CC
ति <u>भ</u>				Vert 3	8 0	ariz.
त्य के अन्य के				Vert j		ariz. Net CC
हतु त				Vert 3		ariz.
हतु भ				Vert 3	H	oriz teet CC
हेतु भ					H	oriz Net CG
स्तु भ				Vert 3	H	oriz Net CG
14 84 84 84 84 84 84 84 84 84 84 84 84 84				Vert 1	H	29C
2 2 2 2 2 2 2 2				Vert 3		oriz 1964 (10 1984 - 10 1984 - 10 1995 - 10 19 1995 - 10 1995 - 10
14 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8				Vert 3		oriz New ''C - 300 - 290
A P				Vert 3		290 280
14 31 84 31				Vert 3		oriz her ^C 300 290
4 3 4 3				Vert 3		280
24 24 25 25 24				Vert 3		2300 2290
A S				Vert 1		270
4 31 8 31				Vert 1		270
IT I						280 2270
						280 260
GROUND				Vert 3		280 260
GROUND						2300 2290 280 270
GROUND				Vert 3		250 - 250 -
GROUND						250 - 250 -
GROUND						250 - 250 -
GROUND						250
GROUND						250
GROUND						250



ARUPPAL & BOBER MAT . NAMES IL

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MBLEK 1978

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Res manufactors



APPENDIX F: SELECTED PHOTOS



Photo taken at TH13-005 on the main runway looking south.



Photo taken at TH13-006 on the main runway looking west at the crosswind runway.



Photo taken at TH13-013, and soil core sampled from 15 to 20 feet in depth.



Photo taken at TH13-016, and soil core sampled from 15 to 20 feet in depth.



Photo taken at TH13-022, and soil core sampled from 0 to 2.5 feet in depth.



Photo taken at TH13-022, and soil core sampled from 5 to 10 feet in depth.



Photo taken at TH13-022, and soil core sampled from 10 to 15 feet in depth.



Photo taken at TH13-022, and soil core sampled from 15 to 20 feet in depth.



Photo taken at TH13-050, and soil core sampled from 10 to 15 feet in depth.



Photo taken at TH13-050, and soil core sampled from 15 to 20 feet in depth.



Photo taken at the existing SREB building and looking south toward proposed new airport access road realignment area.



Photo taken at the existing aircraft parking apron and looking north.

APPENDIX G: SYMBOLS AND DEFINITIONS, UNIFIED SOIL CLASSIFICATION SYSTEM, DESCRIPTION AND CLASSIFICATION OF FROZEN SOILS



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<u>Classification of Soils for Engineering Purposes (Unified Soil Classification System)</u>

Flow Chart for Classifying Fine-Grained Soil (50% or More Passes No. 200 Sieve)



Flow Chart for Classifying Organic Fine-Grained Soil (50% or More Passes No. 200 Sieve)



Cu≥4 and 1<Cc≤3

Cu<4 and/or 1>Cc>3

Flow Chart for Classifying Coarse-Grained Soil (More Than 50% Retained on No. 200 Sieve)

GROUP SYMBOL

GW

+ <15% seed

<u>>15%</u> sond

<157 sond

GROUP NAME

- Well-graded gravel - Well-graded gravel with sand

Poorly graded gravel with sand

- Poorly groded grovel



Pad I				_	and the second se			
Description of Soil Phase (a) (Independent of Frozen State)	DESCRIPTION AND CLASSIFICATION OF FROZEN SOILS							
Part II <u>Description of</u> <u>Frozen Soil</u>	Major Group		Sub-Group				Guide for Construction on Soils Subject to Freezing and Thawing	
	Description (2)	Designation (3)	Description (4)	Designation (5)	Field Identification (6)	Pertinent Properties of Frozen Materials which may be measured by physical tests to supplement field identification. (7)	Thaw Characteristics (8)	Criteria (9)
	Segregated ice is not visible by eye (b) Segregated ice is visible by eye. (Ice 1 inch or less in thickness) (b)	N V .	Poorly Bonded or Friable	Nf	Identify by visual examination. To determine presence of excess ice, use procedure under note (c) below and hand magnifying lens as necessary. For soils not fully saturated, estimate degree of ice saturation: Medium, Low. Note presence of crystals, or of ice coatings around larger particles. For ice phase, record the following as applicable: Location Size Orientation Shape Thickness Spacing Pattern of arrangement Length Hardness } Structure) per part III Below Color } Estimate volume of visible segregated ice present as percent of total sample volume Designate material as ICE (d) and use descriptive terms as follows, usually one item from each group, as applicable: Hardness Structure Color Admixtures Hard Clear e.g.: Soft Cloudy Color- Marking Candied Gray Inclus- crystals) Granular Blue ions	In-Place Temperature Density and Void Ratio a) In Frozen State b) After Thawing in Place Water Content (Total H ₂ 0, including ice) a) Average b) Distribution Strength a) Compressive b) Tensile c) Shear d) Adfreeze Elastic Properties Thermal Properties Thermal Properties Ice Crystal Structure (using optional instruments.) a) Orientation of Axes b) Crystal size c) Crystal shape d) Pattern of Arrangement	Usually Thaw-Stable	The potential intensity of ice segregation in a soil is dependent to a large degree on its void sizes and may be expressed as an empirical function of grain size as follows: Most inorganic soils containing 3 percent or more of grains finer than 0.02 mm in diameter by weight are frost-susceptible. Gravels, well-graded sands and silty sands, especially those approaching the theoretical maximum density curve, which contain 1.5 to 3 percent finer than 0.02 mm by weight without being frost-susceptible. However, their tendency to occur interbedded with other soils usually makes it impractical to consider them separately. Soils classed as frost-susceptible under the above criteria are likely to develop significant ice segregation and frost heave if frozen at normal rates with free water readily available. Soils so frozen will fall into the thaw-unstable category. However, they ma also be classed as thaw-stable if frozen with insufficient water to permit ice segregation.
			No excess ice Well Bonded	n Nb e				
			Excess ice					
			crystals or inclusions	Vx			Usually Thaw-Unstable	
			Ice coatings on particles	Vc				
			Random or irregularly oriente ice formations	d Vr				
			Stratified or distinctly oriented ice formations	s Vs				Soils classed as non-frost-susceptible (*NFS) under the above criteria usually occur without significant ice segregation and are not exact and may be inadequate for some structure applications exceptions may also result from minor soil variations.
Part III <u>Description of</u> <u>Substantial Ice</u> <u>Strata</u>	Ice (Greater than 1 inch in thickness)	lce	Ice with soil inclusions	lce + Soil Type				
			Ice without soil inclusions	lce		Same as Part II above, as applicable, with special emphasis on Ice Crystal Structure	•	In permafrost areas, ice wedges, pockets, veins, or other ice bodies may be found whose mode of origin is different from that described above. Such ice may be the result of long-time surface expansion and contraction phenomena or may be glacial or othe lice which has been buried under a protective earth cover.

EFINITIONS

Ice Coatings on Particles are discernible layers of ice found on or below the larger soil Well-bonded signifies that the soil particles are strongly held together by the ice and that the frozen soil possesses relatively high resistance to chipping or breaking. particles in a frozen soil mass. They are sometimes associated with hoarfrost

crystals, which have grown into voids produced by the freezing action. Ice Crystal is a very small individual ice particle visible in the face of a soil mass. Crystals may be present alone or in a combination with other ice formations.

Clear ice is transparent and contains only a moderate number of air bubbles.(e) Cloudy Ice is translucent, but essentially sound and non-pervious

Porous Ice contains numerous voids, usually interconnected and usually resulting from melting at air bubbles or along crystal interfaces from presence of salt or other nor produce detrimental settlement. materials in the water, or from the freezing of saturated snow. Though porous, the mass retains its structural unity.

very loosely bonded together.

Granular Ice is composed of coarse, more or less equidimensional, ice crystals weakly bonded together.

Ice Lenses are lenticular ice formations in soil occurring essentially parallel to each other, generally normal to the direction of heat loss and commonly in repeated layers.

Ice Segregation is the growth of ice as distinct lenses, layers, veins and masses in soils, commonly but not always oriented normal to direction of heat loss

Poorly-bonded signifies that the soil particles are weakly held together by the ice and that the frozen soil consequently has poor resistance to chipping or breaking.

Friable denotes a condition in which material is easily broken up under light to moderate pressure.

Thaw-Stable frozen soils do not, on thawing, show loss of strength below normal, long-time thawed values However, the impression to the unaided eye is that none of the

Thaw-Unstable frozen soils show on thawing, significant loss of strength below normal, long-time thawed (c) When visual methods may be inadequate, a simple field test Candled ice is ice which has rotted or otherwise formed into long columnar crystals, values and/or significant settlement, as a direct result of the melting of the excess ice in the soil.

> Modified from: Linell, K. A. and Kaplar, C. W., 1966, Description and Classification of Frozen Soils, Proc. International Conference on Permafrost (1963), Lafayette, IN, U.S. National Academy of Sciences, Publ. 1287, pp 481-487.

NOTES:

(a) When rock is encountered, standard rock classification terminology should be used. (b) Frozen soils in the N group may on close examination indicate presence of ice within the voids of the material by crystalline reflections or by a sheen on fractured or trimmed surfaces. frozen water occupies space in excess of the original voids in the soil. The opposite is true of frozen soils in the V group. to aid evaluation of volume of excess ice can be made by placing some frozen soil in a small jar, allowing it to melt and observing the quantity of supernatant water as a percent of total volume.

(d) Where special forms of ice, such as hoarfrost, can be distinguished, more explicit description should be given. (e) Observer should be careful to avoid being misled by surface scratches or frost coating on the ice.